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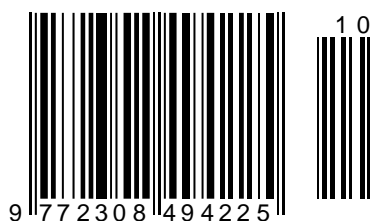
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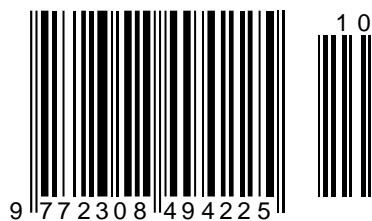
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SOME CHARACTERISTICS OF NANOFIBER NANOPOROUS MATERIALS

Abstract: The article presents the results of a study on the production of nanofibre anisotropic nanoporous materials based on silk fibroin (FS) and Acrylonitrile Copolymer (Co-An) of nanofibers in the form of a thin material. The dependence of the anisotropy, which characterizes the structural states of the obtained thin-layer polymeric materials, on the deformation effects, their sorption and filtration properties has been studied. Wide possibilities of using nanofiber nonwoven materials as nanofilters and the efficiency of the filtration process of nonwoven materials with an increase in the size of their nanopores.

Key words: nanofiber, nanomaterial, formation, polymer, structure, temperature.

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НЕКОТОРЫЕ ХАРАКТЕРИСТИКИ НАНОВОЛОКОННЫХ НАНОПОРИСТЫХ МАТЕРИАЛОВ

Аннотация: В статье представлены результаты исследований по производству нановолоконных анизотропных нанопористых материалов на основе фиброина шелка (ФС) и сополимера акрилонитрила (Co-An) нановолокон в виде тонкого материала. Исследована зависимость анизотропии, характеризующей структурные состояния полученных тонкослойных полимерных материалов, от деформационных воздействий, их сорбционных и фильтрационных свойств. Широкие возможности использования нановолоконных нетканых материалов в качестве нанофильтров и эффективность процесса фильтрации нетканых материалов с увеличением размера их нанопор.

Ключевые слова: нановолокно, наноматериал, формирование, полимер, структура, температура.

Введение

Динамичное развитие современной наноауки и нанотехнологии тесно связано со созданием новых наноматериалов, в частности, нановолокон полимеров с уникальными свойствами [1]. Нановолокна формируют из прядильных растворов и расплавов полимеров путем вытягивания жидкой струи посредством сильного электрического поля, т.е. методом электроформования (электроспиннинга) [2].

Метод основан на осуществление превращения «струя-нановолокно» в воздухе между анода (фильера) до катода (барабан или экран). Высокое напряжение, подаваемое на анод не только вытягивает молекул полимеров из струи в направлении катода, но и осуществляет ориентационно-скрученное структурообразование макромолекул в форме нановолокон [3]. Технически принятие нановолокон на стационарный экран является

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простым, что позволяет непосредственной укладке формируемого нановолокна на поверхность экрана в виде нетканого материала. Причем, полученный нетканый материал характеризуется нанопористостью [4].

Характеристики нановолоконных нетканых материалов и их нано пористость во многом зависит от условий электроспиннинга и укладки нановолокон на поверхности экрана – приемника [5]. В этом большой интерес представляет получение нановолоконных нанопористых нетканых материалов на основе местных биосовместимых полимеров, в частности, фиброина и целлюлозы, выделенных, соответственно, из отходов переработки кокона шелка и хлопкового сырья, например, лигнина. Нановолокна фиброина характеризуются с выраженной био- активностью, которой наиболее ярко проявляется на поверхностном слое нанопористого нетканого материала. Внутри таких материалов нановолокна находится в произвольно-уплотненной форме, т.е. в неупорядоченном состоянии [6].

В таком случае пространства между нановолокнами образованные поры, нанопоры в том числе, имеют различные размеры и размерности. Поскольку, нановолокна проявляют выраженной поверхностной активности, то это явление в таких разноразмерных порах и нанопорах проявляется различной степени, и главное в зависимости от формы и размеры данных пор проходит через поры различные количества вещества в газообразном и жидкофазном состоянии. Проявление таких разнообразных свойств активности в нановолоконных нетканых материалах усложняют проявление свойств характерных для наноматериала. Например, при практическом применении нановолоконных материалов в качестве биоактивных покрытий открытых ран очень важно наличие в них нанопоры с определенными размерами, способными пропускать через себя определенного объема вещества, воздуха и т.п. Поэтому, целесообразно получение нетканых материалов, в которых поверхностный слой состоял из биоактивных биосовместимых нановолокон и внутри были нанопоры с определенными размерами. Такие нанопористые наноматериалы, безусловно, находят широкое практическое применение в области медицины, фармацевтики, косметологии, текстиля, экологии и т.п [7].

Для получения таких нанопористых материалов необходимо усовершенствование способа (установки и метода) электроспиннинга со специальным устройством приёмника (экрана), способного осуществлять равномерной укладки нановолокон с образованием однотипных нанопор в получаемом нетканом материале.

В целом, усовершенствование способа электроспиннинга нановолокон на уровне нанотехнологии современных материалов, прежде всего, нанопористых нетканых материалов на основе местных много тоннажных биополимеров является весьма актуальным научным направлением прикладных исследований [8].

Выявлено, что в зависимости от условий формования получают нановолокна с толщиной 5 - 500 nm, а толщина нетканого материала может быть регулирована от 10 μm до десятки mm. В случае полиэлектролитов высокое напряжение способствует локализацию мобильных ионогенных групп макромолекул на поверхности нановолокон и в результате полученный нановолоконный нетканый материал обладает выраженной поверхностной активностью [9]. Особое внимание привлекает следующие моменты: - формование нановолокон на основе биополимеров (например, фиброина, коллагена, хитозана), содержащих положительно заряженных аминных групп позволяет получить нетканые бактерицидные материалы, поскольку, аминные группы блокируют отрицательно заряженных бактерий. Такие материалы могут быть применены в качестве биоразлагаемые перевязочные средства или покрытия для открытых ран [10]; - в случае формования нановолокон на основе ионогенных биосовместимых полимеров, в частности, сополимера акрилонитрила (АК:МА:ИК) получают нетканые материалы с высокой гибкостью и выраженной поверхностной активностью, проявляющие взаимодействия с различными веществами. Такие нетканые материалы могут быть использованы в качестве высокоэффективные наночистоты для газообразных и жидкофазных веществ. Исходя из этого исследовали поверхностно-активных свойств нановолокон на основе фиброина шелка и сополимера акрилонитрила [11].

В качестве объектов исследования выбрали волокон фиброин шелка (ФШ), очищенного от серицина и жировосков, а также волокон сополимера акрилонитрила (Со-АН), произведенного в ОАО «Навоиазот». Волокна ФШ растворяли в 50 % CaCl_2 в целях исключения возможных деструкций цепей. Далее, проводили диализ против ионов CaCl_2 , и полученный порошок аморфизированного фиброина растворяли в муравьиной кислоте (HCOOH). Опыты показали, что растворы ФШ с концентрацией $C = 5 - 20\%$ в HCOOH пригодны для получения нановолокон с толщиной 100-300 nm методом электроспиннинга при напряжении 3 - 6 kV/cm.

Прядильные растворы со-АН приготовили в ДМФА с $C = 5 - 10\%$ в ДМФА. Выявлено, что при таком же диапазоне напряжения 3 - 6 kV/cm

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формируются нановолокон со-АН, однако толщина нановолокон при этом колеблется в интервале 50 - 500 nm.

При этом было очевидно концентрирование ионогенных групп макромолекул на поверхности нановолокон, следовательно, проявление выраженных поверхностно-активных свойств их при контакте составляющими (атомами, молекулами, ионами, частицами) окружающей среды. Такие особенности нановолокон исследовали методами физической химии, в частности, сорбции паров, нанофильтрации

жидкостей, электроосмоса ζ -потенциала, а также испытали в качестве биопокрытия [12].

Сорбции паров. Опыты проводили на высоковакуумной установке с ртутными затворами и кварцевыми весами Мак-Бэна при 298 К и остаточном давлении воздуха 10^{-3} - 10^{-4} Па. В качестве сорбата выбрали этанола и воды. Получили типичные S-образные изотермы сорбции, которые приведены на рис.1 в виде зависимости показателя сорбции (x/m) от относительной влажности (P/P_0) для нановолокон фиброина и Со-АН.

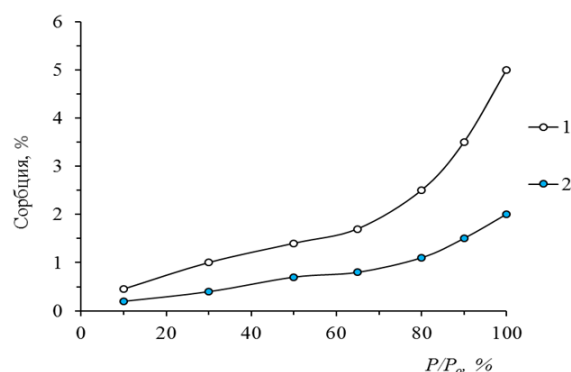


Рис. 1. Изотермы сорбции паров этанола (1, 2) и воды (1', 2') для нановолокон ФШ (1, 1') и со-АН (2, 2').

Видно, что нановолоконные образцы сравнительно больше сорбируют паров воды, чем этанола. Причем, такое явление заметно ярче проявляется в случае образца ФШ. Данное различие по-видимому, обусловлено с плотной упаковкой гибкоцепных молекул со-АН по сравнению жесткоцепных молекул ФШ в нановолокнах. А также наличием сравнительно больших количества гидрофильных групп в цепях ФШ. Подобные различия обнаружили при расчете капиллярно-пористых и структурных показателей нановолокон, а именно, сорбционного объема (X_m), удельной поверхности (S_{y0}), суммарного объема пор (W_0), среднего

радиуса пор (r_k) нановолокон приведены в табл. 1. Видно, что значение показателей сравнительно низкое в случае паров этанола, чем воды как для со-АН, так и для ФШ. Заметно завышенное значение в случае ФШ, т.е. большие объемы пор обусловлены наличием в молекулах фиброина крупных аминокислотных остатков типа аспаргиновых и глутаминовых, которые не укладываются как в α -спиральных, так и в β -структурных формах данного белка в волокнах. Тем не менее радиусы пор достаточно большие для проникновения атомов и не больших молекул в объем нановолокон [13].

Таблица 1. Капиллярно-пористые и структурные показатели нановолокон

Образец	ФШ	Со-АН	ФШ	Со-АН
	Этанол		Вода	
$X_m, g/g$	0,0045	0,0041	0,0054	0,0052
$S_{y0}, m^2/g$	14,72	12,91	23,04	18,33
$W_0, cm^3/g$	0,028	0,020	0,042	0,037
$r_k, \text{Å}$	38,27	31,41	45,26	36,55

Таким образом, из полученных результатов следуют, что нановолокна ФШ и со-АН являются наноматериалов, способных сорбировать паров атомов и молекул с размерами не более 30-40 Å

сохраняя свои формы без существенных деформационных изменений [14].

Нанофильтрация. Безусловно, нетканые нанопористые материалы на основе поверхностно-активных нановолокон проявляют

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специфические взаимодействия с газообразными и жидкофазными веществами, и могут селективно фиксировать или удерживать их составляющих в зависимости от химической природы, строения и размерности. Такая селективность наиболее ярко проявляется, когда через поверхностно-активный нанопористый материал пропускается коллоидная и молекулярно-дисперсная система.

Это обуславливало проведения настоящего опыта в целях выявления эффективности нановолоконного нанопористого материала со-АН в качестве нанофильтра, пропускающая через него отработанного машинного масла, содержащего микро- и наноразмерных частиц. Причем, машинное масло является химически нейтральным относительно нановолокон со-АН. Это дало дополнительная возможность для проведения сравнительных опытов образцов нетканого материала со-АН, различающихся по размерам пор: 50, 100, 300 нм. При этом толщина нетканого материала составляла $d_n = 0,5$ мм.

Исследование проводили следующим образом, т.е. через нанофильтр массой (m_n), находящийся в длительном воронке, пропустили

$m_o = 100$ ml отработанного машинного масла, имеющего коричневого цвета. На выходе, т.е. после протекания масла через нанофильтр имело светло-желтый цвет и масса его уменьшалась (m_i), т.е. определенная часть массы (m_p) из состава удержалась на нанофилтре. Это свидетельствовало о протекании фильтрации масла, которая протекала интенсивно в течение 60-80 min. При этом эффективность фильтрации судили по отношению m_i/m_o по времени (t) наблюдения, построив графики, представленные на рис.2. Видно, что процесс фильтрации носит кинетический характер, т.е. с увеличением времени и размеров нанопор масса продукта фильтрации (m_i) повышается монотонно до 60-80 min, далее стабилизируется. Причем, уменьшение размеров поры нанофильтра способствует росту эффективности удержания примесей. Выявлено, что степень очистки отработанного машинного масла при пропускании через нанофильтры без всяких внешних давлений или деформационных воздействий составляет примерно 25 % в случае использования нанопоры 80 нм, почти 65 % в случае нанопоры 50 нм.

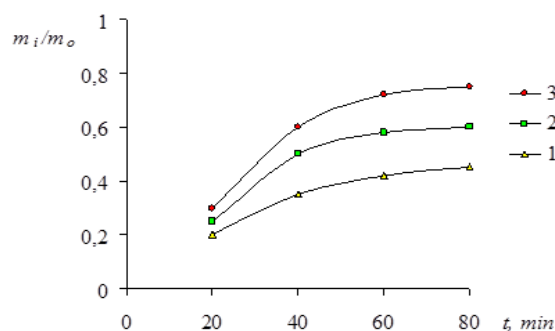


Рис.2. Зависимость относительной изменения массы (m) от времени (t) при пропускании машинного масла через нанофильтры Со-АН с различными размерами пор: 1 – 50 нм, 2 – 100 нм, 3 – 300 нм.

Это в принципе хороший результат для рекомендации нановолоконного нетканого нанопористого материала на основе Со-АН на практическое применение в качестве нанофильтров.

Электроосмос. Взаимодействие поверхностно-активных нановолоконных нетканых материалов с ионами металлов исследовали с помощью метода электроосмоса [15]. При этом в качестве нанопористой мембраны использовали нановолоконного нетканого материала на основе ФШ и подвижной дисперсной фазы водного раствора CuSO_4 (2%). Определяли значения ζ -потенциала, характеризующего устойчивости взаимодействия ионов с функциональными группами нановолокон

при перемещении дисперсной среды через мембраны под действием постоянного тока (рис.3.). Выявлено, что значение ζ -потенциала повышается от 40 до 80 mV при росте концентрации CuSO_4 от 0,5 до 2 %. Данные результаты свидетельствуют об устойчивости взаимодействий ионов с элементами нановолокон из-за поверхностной активности нетканого материала.

Таким образом, результаты показывают, что на основе фиброина возможно получение нановолоконных нетканых материалов с поверхностно-активными свойствами, достаточно устойчиво взаимодействующие и удерживающие ионы металлов в дисперсных средах.

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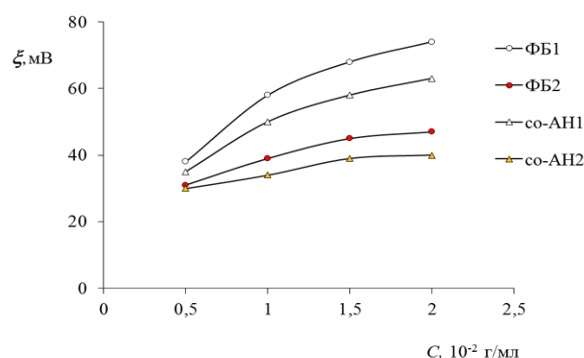


Рис.3. Зависимость значения ζ -потенциала от концентрации (C) раствора CuSO_4 для нановолоконного нетканого материала на основе ФШ.

Нановолоконные биопокрытия.

Поверхностно-активные нетканых материалы на основе Co-АН является биосовместимым, а на основе ФШ не только биосовместимым, но и биоактивным. Это представляло интерес проведения медико-биологических испытаний, например, в качестве покрытия открытых ран. Для этого из нановолоконных материалов Co-АН и ФШ нарезали квадратики с размерами $2 \times 2 \text{ см}^2$ и согласно [16] проводили стерилизации посредством этилового спирта. Далее, в медико-биологическом лабораторном условии на поверхность открытых ран у крыс наложили квадратиков и фиксировали их с краев посредством пластыров. Сравнительные наблюдения за заживлением ран проводили в прочих равных условиях с использованием для каждого образца наноматериалов по 10 крыс в течение 30 дней.

Результаты наблюдения обнаружили, что заживление открытых ран в случае использования биоактивных наноматериалов протекало значительно интенсивнее, чем биосовместимого образца. Биоактивные нанопокрытия способствовали практически полному заживлению ран в течение 14 суток, тогда как заживление ран при биосовместимом образце продолжалось до 21 суток. В конце заживления ран наноматериальные покрытия отпадали без всяких дополнительных усилий [17]. Отделившие от ран наноматериалы были анализированы на предмет сохранности структуры. Поляризационно-оптические и электронно-микроскопические наблюдения показали, что в целом нановолоконные структуры образцов сохранились. Контрольные наблюдения за физическим и медико-биологическим состоянием заживленных участков крыс, проведенные в

течение трех месяцев не характеризовались с каким-либо серьезным структурным изменением [18].

Таким образом, испытания нановолоконных материалов Co-АН и ФШ показали принципиальной возможности их применения в качестве покрытий открытых ран. На основе проведенных исследований показано, что на основе фиброина шелка и сополимера акрилонитрила, имеющих функционально-активных групп возможно получение нановолоконных нетканых материалов с выраженными поверхностно-активными свойствами. Исследование данных материалов на предмет выявления сорбционных характеристик, фильтрующих способностей, электрокинетических устойчивостей, биоактивных покрытий дали положительные результаты, на основе которых на последующем этапе возможна разработки наноматериалов со специальными свойствами [19].

ЗАКЛЮЧЕНИЕ

Определены некоторые физико-химические и медико-биологические характеристики нановолоконных нанопористых нетканых материалов, необходимые для практического применения. В частности, выявлены сорбционные характеристики, фильтрующие способности, электрокинетические устойчивости, которые имеют важные значения для разработки нановолоконных нетканых материалов. Повышенное значение электрокинетического потенциала выше $\pm 30 \text{ мВ}$ показало стабильность и устойчивость взаимодействия нетканых анизотропных материалов с ионами электролита, со специальными свойствами.

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Article



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REFERENCE DATA OF PRESSURE DISTRIBUTION ON THE SURFACES OF AIRFOILS HAVING THE NAMES BEGINNING WITH THE LETTER M

Abstract: The results of the computer calculation of air flow around the airfoils having the names beginning with the letter M are presented in the article. The contours of pressure distribution on the surfaces of the airfoils at the angles of attack of 0, 15 and -15 degrees in conditions of the subsonic airplane flight speed were obtained.

Key words: the airfoil, the angle of attack, pressure, the surface.

Language: English

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Introduction

Creating reference materials that determine the most accurate pressure distribution on the airfoil surfaces is an actual task of the airplane aerodynamics.

Materials and methods

The study of air flow around the airfoils was carried out in a two-dimensional formulation by means of the computer calculation in the *Comsol Multiphysics* program. The airfoils in the cross section were taken as objects of research [1-28]. In this work,

the airfoils having the names beginning with the letter *M* were adopted. Air flow around the airfoils was carried out at the angles of attack (α) of 0, 15 and -15 degrees. Flight speed of the airplane in each case was subsonic. The airplane flight in the atmosphere was carried out under normal weather conditions. The geometric characteristics of the studied airfoils are presented in the Table 1. The geometric shapes of the airfoils in the cross section are presented in the Table 2.

Table 1. The geometric characteristics of the airfoils.

Airfoil name	Max. thickness	Max. camber	Leading edge radius	Trailing edge thickness
<i>M06-13-1</i>	12.84% at 33.2% of the chord	5.16% at 33.2% of the chord	0.982%	0.015%
<i>M3 - HB396</i>	9.59% at 31.0% of the chord	2.98% at 47.0% of the chord	0.4853%	0.0%
<i>M6 (65%)</i>	7.81% at 30.0% of the chord	1.44% at 30.0% of the chord	0.4573%	0.0%
<i>M6 (85%)</i>	10.21% at 30.0% of the chord	1.88% at 30.0% of the chord	0.9315%	0.0%
<i>MA409 (original)</i>	6.79% at 25.0% of the chord	4.31% at 40.0% of the chord	0.6961%	0.07%
<i>MA409 (smoothed)</i>	6.69% at 23.8% of the chord	3.33% at 49.3% of the chord	0.4323%	0.07%
<i>Marquardt</i>	11.53% at 20.0% of the chord	7.05% at 40.0% of the chord	1.923%	0.0%
<i>Marsden</i>	27.88% at 31.6% of the chord	9.61% at 34.5% of the chord	7.7426%	0.0%
<i>MARSKE MONARCH</i>	12.22% at 20.0% of the chord	3.38% at 15.0% of the chord	1.9108%	0.0%
<i>MARSKE PIONEER IA</i>	12.05% at 25.0% of the chord	2.69% at 15.0% of the chord	1.7183%	0.0%
<i>MARSKE PIONEER IID ROOT</i>	12.06% at 30.0% of the chord	2.76% at 15.0% of the chord	1.5706%	0.0%
<i>MARSKE PIONEER IID TIP</i>	10.19% at 20.0% of the chord	2.82% at 15.0% of the chord	1.4576%	0.0%
<i>MARSKE XM-1D</i>	13.99% at 24.9% of the chord	3.03% at 24.9% of the chord	2.357%	0.0%
<i>Martin M 1</i>	8.8% at 30.0% of the chord	0.0% at 0.0% of the chord	0.8135%	0.0%
<i>MATWIES6</i>	6.0% at 20.0% of the chord	8.3% at 40.0% of the chord	2.7985%	0.3%
<i>MB253515</i>	14.96% at 35.0% of the chord	2.43% at 37.5% of the chord	1.42%	0.0%
<i>MB253515 15,0% smoothed</i>	14.96% at 35.0% of the chord	2.43% at 37.5% of the chord	1.42%	0.0%
<i>MB303515</i>	14.96% at 35.0% of the chord	2.98% at 35.0% of the chord	1.65%	0.38%
<i>mb7136</i>	7.04% at 26.1% of the chord	1.22% at 38.4% of the chord	0.4918%	0.048%
<i>mb714</i>	7.0% at 26.1% of the chord	1.45% at 38.4% of the chord	0.5224%	0.0477%

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<i>mc813</i>	8.0% at 25.8% of the chord	1.35% at 39.4% of the chord	0.4826%	0.0482%
<i>md8135</i>	8.01% at 28.8% of the chord	1.37% at 38.5% of the chord	0.4021%	0.047%
<i>md814</i>	8.0% at 26.3% of the chord	1.45% at 38.5% of the chord	0.4461%	0.0464%
<i>MEG 59</i>	10.95% at 30.0% of the chord	4.69% at 50.0% of the chord	1.1117%	0.0%
<i>MEG 62-63137</i>	13.68% at 30.0% of the chord	5.86% at 50.0% of the chord	1.5737%	0.0%
<i>MEG 64</i>	7.91% at 40.0% of the chord	2.55% at 20.0% of the chord	0.5884%	0.0%
<i>MEG 66</i>	9.71% at 40.0% of the chord	3.11% at 40.0% of the chord	0.5686%	0.0%
<i>MEG 69-012</i>	11.92% at 40.0% of the chord	0.05% at 70.0% of the chord	1.5272%	0.0%
<i>MEG-197</i>	10.0% at 30.0% of the chord	4.41% at 50.0% of the chord	0.9064%	0.0%
<i>MG 08</i>	8.67% at 30.2% of the chord	2.0% at 35.2% of the chord	0.5949%	0.0%
<i>MG05</i>	9.0% at 26.7% of the chord	0.0% at 0.0% of the chord	0.4237%	0.0%
<i>MG06</i>	7.37% at 22.4% of the chord	1.94% at 31.8% of the chord	0.4307%	0.0%
<i>MH 102</i>	17.0% at 27.7% of the chord	2.9% at 37.6% of the chord	2.006%	0.0%
<i>MH 104</i>	15.24% at 26.4% of the chord	1.92% at 31.0% of the chord	1.2786%	0.0%
<i>MH 106</i>	13.08% at 27.3% of the chord	0.92% at 27.3% of the chord	1.0054%	0.0%
<i>MH 108</i>	11.97% at 22.8% of the chord	1.05% at 18.7% of the chord	1.0607%	0.0%
<i>MH 110</i>	10.02% at 23.9% of the chord	1.07% at 15.8% of the chord	0.7333%	0.0%
<i>MH 112</i>	16.23% at 26.9% of the chord	7.16% at 48.8% of the chord	2.8472%	0.0%
<i>MH 113</i>	14.63% at 27.5% of the chord	6.86% at 49.4% of the chord	1.7997%	0.0%
<i>MH 114</i>	13.04% at 28.1% of the chord	6.51% at 50.0% of the chord	1.1733%	0.0%
<i>MH 115</i>	11.07% at 29.8% of the chord	5.51% at 46.0% of the chord	1.1499%	0.0%
<i>MH 116</i>	9.85% at 32.4% of the chord	4.03% at 48.5% of the chord	0.7086%	0.0%
<i>MH 117</i>	9.81% at 29.1% of the chord	2.69% at 44.6% of the chord	0.7948%	0.0%
<i>MH 18</i>	11.12% at 36.8% of the chord	2.77% at 36.8% of the chord	0.6678%	0.0%
<i>MH 18 11,14%</i>	11.12% at 36.8% of the chord	2.77% at 36.8% of the chord	0.6678%	0.0%
<i>MH 18B</i>	11.73% at 39.6% of the chord	1.95% at 39.6% of the chord	0.7392%	0.0%
<i>MH 20</i>	9.01% at 32.2% of the chord	2.0% at 32.3% of the chord	0.6162%	0.0%
<i>MH 20 9,02%</i>	9.01% at 32.2% of the chord	2.0% at 37.3% of the chord	0.6162%	0.0%
<i>MH 22</i>	7.2% at 27.0% of the chord	1.77% at 37.0% of the chord	0.5245%	0.0%

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OAJI (USA) = 0.350

MH 22 7,21%	7.2% at 27.0% of the chord	1.77% at 37.0% of the chord	0.5245%	0.0%
MH 22-Mod,3	8.31% at 23.7% of the chord	1.6% at 27.9% of the chord	0.629%	0.0%
MH 23	8.0% at 37.5% of the chord	1.24% at 37.5% of the chord	0.5601%	0.0%
MH 24	9.0% at 37.2% of the chord	1.27% at 37.2% of the chord	0.5988%	0.0%
MH 25	9.97% at 42.2% of the chord	1.42% at 37.1% of the chord	0.6179%	0.0%
MH 26	10.98% at 42.3% of the chord	1.47% at 42.3% of the chord	0.6642%	0.0%
MH 27	11.98% at 42.4% of the chord	1.46% at 42.4% of the chord	0.7217%	0.0%
MH 30	7.82% at 31.0% of the chord	1.71% at 46.4% of the chord	0.3675%	0.0%
MH 31	7.98% at 26.9% of the chord	1.16% at 36.7% of the chord	0.4065%	0.0%
MH 32	8.71% at 30.2% of the chord	2.36% at 40.4% of the chord	0.5978%	0.0%
MH 33	7.25% at 26.9% of the chord	1.09% at 41.8% of the chord	0.2066%	0.0%
MH 34	8.5% at 31.7% of the chord	1.12% at 41.8% of the chord	0.2864%	0.0%
MH 42	9.02% at 30.9% of the chord	2.09% at 35.9% of the chord	0.4615%	0.0%
MH 42 8,94%	8.91% at 31.3% of the chord	1.84% at 36.3% of the chord	0.6285%	0.0%
MH 43	8.48% at 31.4% of the chord	1.72% at 36.4% of the chord	0.4127%	0.0%
MH 43 8,5%	8.48% at 31.4% of the chord	1.72% at 36.4% of the chord	0.6073%	0.0%
MH 44	9.66% at 27.1% of the chord	1.48% at 36.9% of the chord	0.7889%	0.0%
MH 45	9.84% at 26.9% of the chord	1.64% at 36.6% of the chord	0.6074%	0.0%
MH 46	11.34% at 27.2% of the chord	1.86% at 37.0% of the chord	1.0004%	0.0%
MH 49	10.49% at 28.8% of the chord	0.7% at 33.6% of the chord	0.7512%	0.0%
MH 60	10.07% at 26.9% of the chord	1.76% at 36.6% of the chord	0.5939%	0.0%
MH 60 10,08%	10.07% at 26.9% of the chord	1.76% at 36.6% of the chord	0.7573%	0.0%
MH 61	10.26% at 27.6% of the chord	1.47% at 37.3% of the chord	0.5093%	0.0%
MH 61 10,28%	10.26% at 27.6% of the chord	1.47% at 37.3% of the chord	0.6511%	0.0%
MH 62	9.29% at 26.9% of the chord	1.59% at 36.6% of the chord	0.5424%	0.0%
MH 62 9,3%	9.29% at 26.9% of the chord	1.59% at 36.6% of the chord	0.691%	0.0%
MH 64	8.6% at 26.9% of the chord	1.44% at 36.7% of the chord	0.4691%	0.0%
MH 78	14.43% at 22.1% of the chord	2.63% at 17.9% of the chord	2.2038%	0.0%
MH 91	15.0% at 27.2% of the chord	1.62% at 14.9% of the chord	1.5419%	0.0%

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<i>MH 92</i>	15.5% at 27.4% of the chord	1.62% at 15.0% of the chord	1.6058%	0.0%
<i>MH 93</i>	15.99% at 27.5% of the chord	1.61% at 15.1% of the chord	2.2627%	0.0%
<i>MH32 (8,71%)</i>	8.71% at 30.2% of the chord	2.36% at 40.4% of the chord	0.4025%	0.0%
<i>MH45</i>	9.84% at 26.9% of the chord	1.64% at 36.6% of the chord	0.6074%	0.0%
<i>mhmi2</i>	9.31% at 23.7% of the chord	2.4% at 27.2% of the chord	0.8483%	0.0001%
<i>mhmi3</i>	9.59% at 25.1% of the chord	2.03% at 30.5% of the chord	0.9763%	0.0005%
<i>MILEY M06-13-128</i>	12.84% at 33.2% of the chord	5.16% at 33.2% of the chord	0.6521%	0.0%
<i>MIRAGE</i>	12.16% at 30.0% of the chord	2.97% at 30.0% of the chord	1.1514%	0.4%
<i>Miser</i>	9.0% at 30.0% of the chord	6.0% at 40.0% of the chord	0.8044%	0.0%
<i>Misto 50-50 S1046-S8035</i>	15.48% at 30.8% of the chord	0.0% at 0.0% of the chord	1.4846%	0.0%
<i>mjp711f-3</i>	7.0% at 28.1% of the chord	1.33% at 100.0% of the chord	0.3588%	0.0421%
<i>mjp712</i>	7.0% at 28.1% of the chord	1.19% at 31.7% of the chord	0.3571%	0.0427%
<i>mjz 1211</i>	12.0% at 28.6% of the chord	1.11% at 25.4% of the chord	1.215%	0.0729%
<i>MM 007</i>	7.0% at 28.3% of the chord	0.06% at 0.0% of the chord	0.3153%	0.0%
<i>MM 008</i>	8.0% at 28.3% of the chord	0.01% at 100.0% of the chord	0.3975%	0.0%
<i>MM 009</i>	9.01% at 27.4% of the chord	0.01% at 100.0% of the chord	0.5503%	0.0%
<i>MM 010</i>	10.0% at 27.5% of the chord	0.01% at 100.0% of the chord	0.6236%	0.0%
<i>MM 012</i>	12.0% at 29.5% of the chord	0.09% at 0.0% of the chord	0.743%	0.0%
<i>MM 1,75-10</i>	9.9% at 30.3% of the chord	1.75% at 30.3% of the chord	0.1442%	0.0%
<i>MM 1,75-9</i>	9.0% at 30.3% of the chord	1.75% at 30.3% of the chord	0.1276%	0.0%
<i>MM 100</i>	8.76% at 28.4% of the chord	2.12% at 39.8% of the chord	0.4966%	0.497%
<i>MM 1010a</i>	10.07% at 32.6% of the chord	0.99% at 40.8% of the chord	0.5668%	0.0%
<i>MM 1010b</i>	10.0% at 34.3% of the chord	1.0% at 37.5% of the chord	0.4879%	0.0%
<i>MM 1100</i>	11.0% at 34.5% of the chord	2.01% at 40.6% of the chord	0.3457%	0.0%
<i>MM 11-29</i>	11.0% at 28.3% of the chord	0.1% at 0.0% of the chord	0.5832%	0.0%
<i>MM 1200</i>	12.0% at 34.5% of the chord	2.01% at 40.6% of the chord	0.4572%	0.0%
<i>MM 1300</i>	13.0% at 35.1% of the chord	2.5% at 43.1% of the chord	0.8675%	0.0%
<i>MM 1407</i>	6.99% at 28.5% of the chord	1.45% at 38.0% of the chord	0.345%	0.0%
<i>MM 1608</i>	7.97% at 29.7% of the chord	1.61% at 37.6% of the chord	0.4272%	0.0%

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<i>MM 1609</i>	9.8% at 29.4% of the chord	1.67% at 29.4% of the chord	1.0429%	0.0003%
<i>MM 1710</i>	10.74% at 28.1% of the chord	1.67% at 35.2% of the chord	0.9755%	0.0001%
<i>MM 1711</i>	11.12% at 30.5% of the chord	1.72% at 32.2% of the chord	0.9869%	0.0005%
<i>MM 1809</i>	9.2% at 27.7% of the chord	1.8% at 34.9% of the chord	0.9012%	0.0004%
<i>MM 1810</i>	10.35% at 30.1% of the chord	1.8% at 36.7% of the chord	0.6071%	0.5%
<i>MM 1811b</i>	11.0% at 30.3% of the chord	1.79% at 35.2% of the chord	0.671%	0.0232%
<i>MM 1910</i>	10.35% at 33.3% of the chord	1.94% at 36.5% of the chord	0.5014%	0.0%
<i>MM 1995</i>	9.6% at 30.3% of the chord	1.93% at 36.8% of the chord	0.4921%	0.0003%
<i>MM 200</i>	9.44% at 28.2% of the chord	2.14% at 40.2% of the chord	0.7986%	0.0%
<i>MM 2-10 a</i>	9.91% at 30.0% of the chord	2.0% at 30.0% of the chord	0.159%	0.0%
<i>MM 2-12</i>	11.89% at 30.0% of the chord	2.0% at 30.0% of the chord	0.2116%	0.0%
<i>MM 2-9</i>	9.01% at 30.0% of the chord	2.0% at 30.0% of the chord	0.1405%	0.0%
<i>MM 300</i>	9.8% at 30.2% of the chord	1.7% at 36.7% of the chord	0.4676%	0.0%
<i>MM 400</i>	10.2% at 28.6% of the chord	2.2% at 40.5% of the chord	0.4601%	0.0%
<i>Mosca 317</i>	10.2% at 30.0% of the chord	5.63% at 10.0% of the chord	1.7382%	0.0%
<i>MRC-16</i>	13.9% at 34.5% of the chord	3.12% at 38.5% of the chord	1.1618%	0.0745%
<i>MRC-20</i>	15.58% at 38.8% of the chord	2.93% at 46.7% of the chord	1.3632%	0.05%
<i>ms1,9-8,7</i>	8.78% at 30.0% of the chord	1.97% at 40.0% of the chord	0.4048%	0.0%
<i>ms2-9,5</i>	9.5% at 30.0% of the chord	2.02% at 40.0% of the chord	0.4745%	0.0%
<i>MS3,3-11GP</i>	11.0% at 30.7% of the chord	3.28% at 38.2% of the chord	0.6348%	0.0%
<i>MS3,3-11GPT</i>	11.0% at 30.7% of the chord	3.28% at 32.6% of the chord	0.5725%	0.0%
<i>MS3,3-15GP</i>	15.0% at 30.7% of the chord	3.28% at 38.2% of the chord	1.2257%	0.0%
<i>msa812</i>	8.0% at 26.4% of the chord	1.22% at 33.8% of the chord	0.5487%	0.0996%
<i>MT172</i>	10.0% at 33.1% of the chord	3.03% at 39.7% of the chord	0.3082%	0.277%
<i>MT722</i>	26.27% at 30.0% of the chord	7.97% at 40.0% of the chord	2.6492%	0.728%
<i>MVA-101M</i>	7.9% at 30.0% of the chord	3.95% at 30.0% of the chord	0.63%	0.0%
<i>MVA-123</i>	5.3% at 15.0% of the chord	6.55% at 40.0% of the chord	0.84%	0.3%
<i>MVA-123M</i>	5.3% at 15.0% of the chord	6.55% at 40.0% of the chord	0.84%	0.3%
<i>MVA-173</i>	7.7% at 20.0% of the chord	6.3% at 40.0% of the chord	0.7734%	0.2%

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JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

<i>MVA-227</i>	14.6% at 25.0% of the chord	11.65% at 50.0% of the chord	1.7205%	0.3%
<i>MVA-301</i>	9.8% at 25.0% of the chord	10.05% at 30.0% of the chord	1.3932%	0.3%
<i>MVA30175</i>	7.4% at 30.0% of the chord	6.95% at 40.0% of the chord	0.8434%	0.2%
<i>MVA-301M</i>	8.7% at 20.0% of the chord	7.15% at 30.0% of the chord	1.1769%	0.2%
<i>MVA-342</i>	5.5% at 25.0% of the chord	6.65% at 40.0% of the chord	0.8799%	0.3%
<i>MVA-439</i>	7.9% at 30.0% of the chord	5.7% at 40.0% of the chord	0.7004%	0.0%
<i>mve8.516</i>	8.5% at 26.8% of the chord	1.6% at 36.5% of the chord	0.5392%	0.0856%
<i>mve8516 f3</i>	8.5% at 26.8% of the chord	1.6% at 36.5% of the chord	0.5392%	0.0861%
<i>MZ 5411</i>	11.25% at 35.0% of the chord	5.63% at 35.0% of the chord	0.8824%	0.2%
<i>MZ 6409</i>	9.1% at 25.0% of the chord	6.75% at 35.0% of the chord	0.8824%	0.2%

Note:

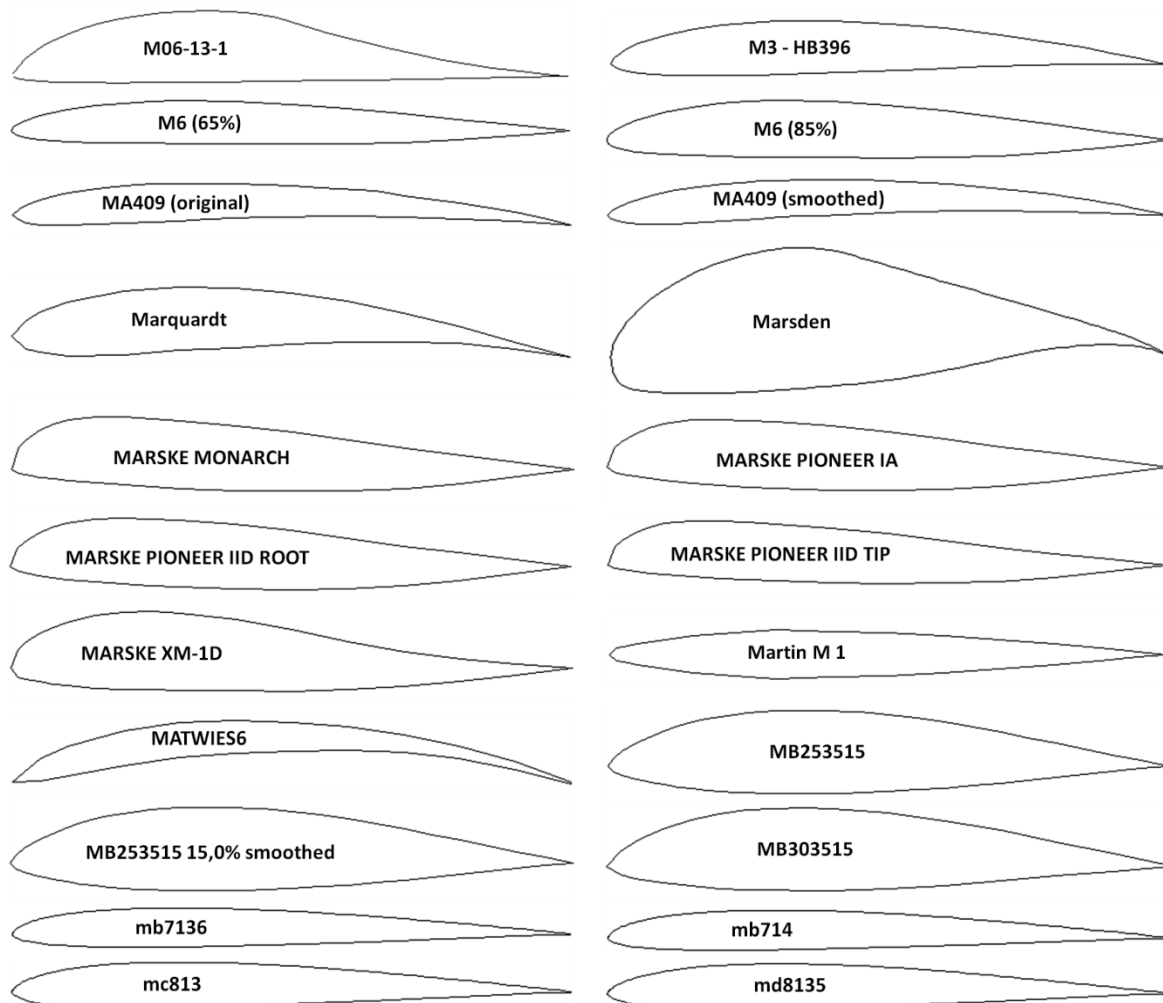
M3 - HB396 (Per HLG-F3J);
Marquardt (J. Marquardt (USA));
Martin M 1 (G.L. Martin (USA));
mb7136 (F5B fast airfoils edumolfino@ciudad.com.ar);
mb714 (F5B fast airfoils edumolfino@ciudad.com.ar);
mc813 (F5B fast airfoils edumolfino@ciudad.com.ar);
md8135 (F5B fast airfoils edumolfino@ciudad.com.ar);
md814 (F5B fast airfoils edumolfino@ciudad.com.ar);
MEG 59 (E. Gallazzi (Italy));
MEG 62-63137 (E. Gallazzi (Italy));
MEG 64 (E. Gallazzi (Italy));
MEG 66 (E. Gallazzi (Italy));
MEG 69-012 (E. Gallazzi (Italy));
MG 08 (Marcel Guwang volet a 30%);
MG05 (Marcel Guwang);
MG06 (Marcel Guwang volets a 30%);
MH 22-Mod,3 (Elaborato per Delta 400);
mhmi2 (By Matteo Gallizia – Italy);
mhmi3 (By Matteo Gallizia – Italy);
mjp711f-3 (Flying Wing airfoils flap 75% - 3 edumol);
mjp712 (edumolfino@ciudad.com.ar);
mjz 1211 (Flying Wing airfoils edumolfino@ciudad.co);
MM 007 (by Mario Marzocchi – Italy);
MM 009 (by Mario Marzocchi – Italy);
MM 010 (by Mario Marzocchi – Italy);
MM 012 (by Mario Marzocchi – Italy);
MM 1,75-10 (by Mario Marzocchi – Italy);
MM 1,75-9 (by Mario Marzocchi – Italy);
MM 100 (by Mario Marzocchi – Italy);
MM 1010b (by Mario Marzocchi – Italy);
MM 1100 (by Mario Marzocchi – Italy);
MM 11-29 (by Mario Marzocchi – Italy);
MM 1200 (by Mario Marzocchi – Italy);
MM 1300 (by Mario Marzocchi – Italy);
MM 1407 (by Mario Marzocchi – Italy);
MM 1608 (by Mario Marzocchi – Italy);

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MM 1710 (by Mario Marzocchi – Italy);
MM 1809 (by Mario Marzocchi – Italy);
MM 1811b (by Mario Marzocchi – Italy);
MM 1910 (by Mario Marzocchi – Italy);
MM 1995 (by Mario Marzocchi – Italy);
MM 200 (by Mario Marzocchi – Italy);
MM 2-10 a (by Mario Marzocchi);
MM 2-12 (by Mario Marzocchi);
MM 2-9 (by Mario Marzocchi – Italy);
MM 300 (by Mario Marzocchi – Italy);
MM 400 (by Mario Marzocchi – Italy);
Mosca 317 (TsAGI (URSS));
ms1,9-8,7 (f3i, f3b matthieu.scherrer@supaero.fr);
ms2-9,5 (f3i, f3b root matthieu.scherrer@supaero.fr);
MS3,3-11GP (thermaling, scale, matthieu.scherrer@su);
MS3,3-11GPT (for tip; thermaling, scale matthieu.sc);
MS3,3-15GP (root of scale sailplane matthieu.scherr);
msa812 (F5B fast airfoils edumolfino@ciudad.com.ar);
mve8.516 (F3B airfoils edumolfino@ciudad.com.ar);
mve8516 f3 (F3B airfoils flap 80% +3 edumolfino@ciudad.com.ar);
MZ 5411 (F. Zaic (USA));
MZ 6409 (F. Zaic (USA)).

Table 2. The geometric shapes of the airfoils in the cross section.



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- md814
- MEG 62-63137
- MEG 66
- MEG-197
- MG05
- MH 102
- MH 106
- MH 110
- MH 113
- MH 115
- MH 117
- MH 18 11,14%
- MH 20
- MH 22
- MH 22-Mod,3
- MH 24
- MH 26
- MH 30
- MH 32
- MH 34
- MH 42 8,94%
- MH 43 8,5%
- MH 45
- MH 49

- MEG 59
- MEG 64
- MEG 69-012
- MG 08
- MG06
- MH 104
- MH 108
- MH 112
- MH 114
- MH 116
- MH 18
- MH 18B
- MH 20 9,02%
- MH 22 7,21%
- MH 23
- MH 25
- MH 27
- MH 31
- MH 33
- MH 42
- MH 43
- MH 44
- MH 46
- MH 60

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IBI (India) = 4.260
OAJI (USA) = 0.350

- MH 60 10,08%
- MH 61 10,28%
- MH 62 9,3%
- MH 78
- MH 92
- MH32 (8,71%)
- mhmi2
- MILEY M06-13-128
- Miser
- mjp711f-3
- mjz 1211
- MM 008
- MM 010
- MM 1,75-10
- MM 100
- MM 1010b
- MM 11-29
- MM 1300
- MM 1608
- MM 1710
- MM 1809
- MM 1811b
- MM 1995

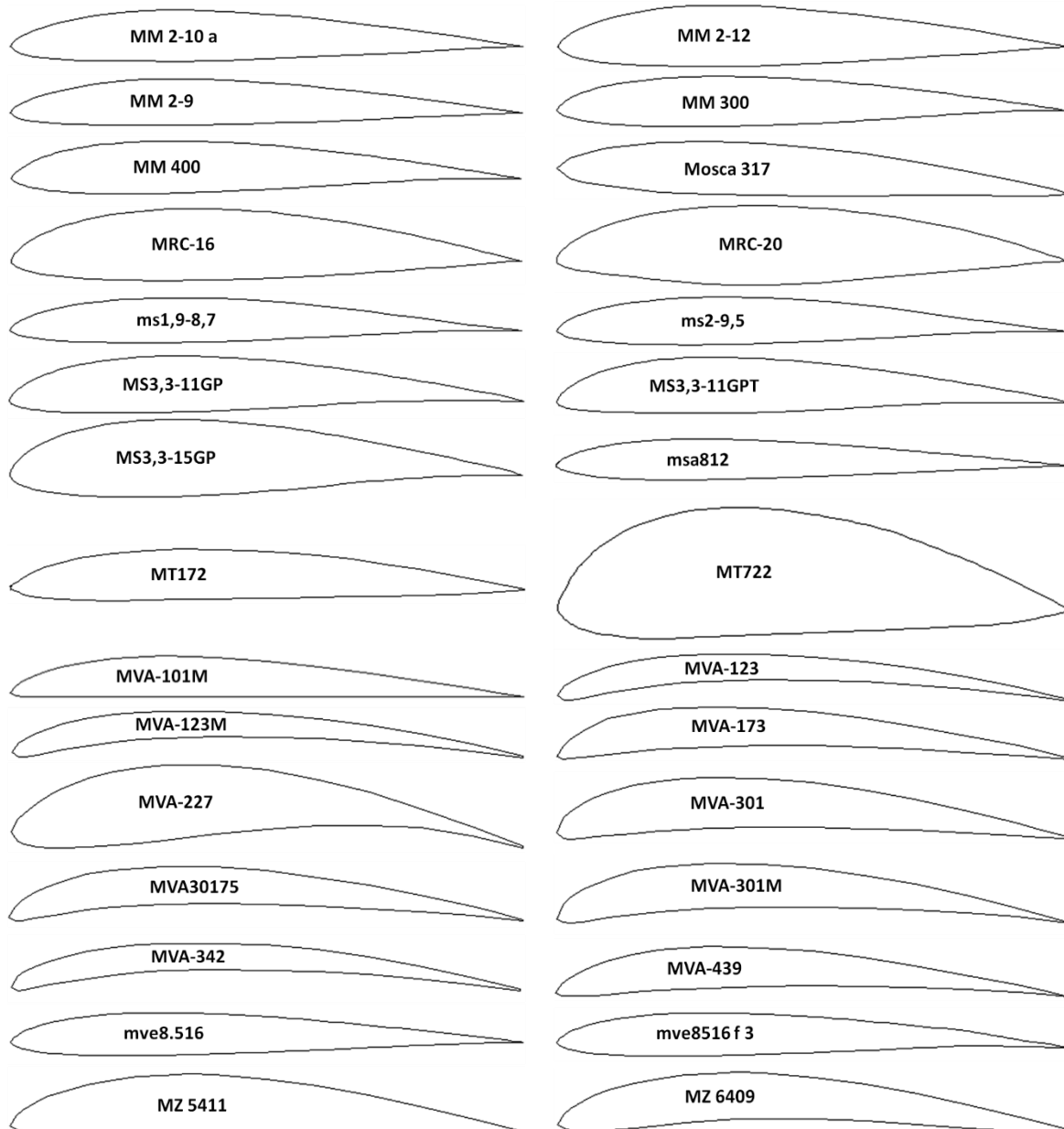
- MH 61
- MH 62
- MH 64
- MH 91
- MH 93
- MH45
- mhmi3
- MIRAGE
- Misto 50-50 S1046-S8035
- mjp712
- MM 007
- MM 009
- MM 012
- MM 1,75-9
- MM 1010a
- MM 1100
- MM 1200
- MM 1407
- MM 1609
- MM 1711
- MM 1810
- MM 1910
- MM 200

Impact Factor:

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 JIF = 1.500

SIS (USA) = 0.912
 ПИИЦ (Russia) = 3.939
 ESJI (KZ) = 8.771
 SJIF (Morocco) = 7.184

ICV (Poland) = 6.630
 PIF (India) = 1.940
 IBI (India) = 4.260
 OAJI (USA) = 0.350



Results and discussion

The calculated pressure contours on the surfaces of the airfoils at the different angles of attack are presented in the Figs. 1-146. The calculated values on the scale can be represented as the basic values when comparing the pressure drop under conditions of changing the angle of attack of the airfoils.

146 airfoils of the airplane wings were considered. All airfoils are asymmetrical, with the exception of the Martin M 1, MG05 and Misto 50-50 S1046-S8035, which are symmetrical.

Aerodynamic characteristics depend on the geometry of the airfoil of the airplane wing. The maximum thickness along the chord is observed for the Marsden (27.88%), the minimum thickness along the chord is observed for the MVA-123 (5.3%) of the considered airfoils. The curved airfoils potentially

have better aerodynamic characteristics. The camber of the MVA-227 airfoil is 11.65% relative to the chord length, which is the highest ratio among all the studied airfoils. The value of the radius of the leading edge of the airfoil affects the drag, i.e. the flight speed of the airplane. The smallest and largest leading edge radii of 0.1276% and 7.7426% were determined for the MM 1.75-9 and Marsden airfoils, respectively. The trailing edge thickness for the most airfoils is 0%. The maximum thickness of the trailing edge (0.728%) was identified for the MT722 airfoil.

Let us consider in detail the change in pressure on the surfaces of several proposed airfoils under conditions of changing the angle of attack: MARSKE MONARCH, Martin M 1, MATWIES6, MEG 64, MH 27, MILEY M06-13-128, MT722 and MVA-227.

Impact Factor:

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GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

The MARSKE MONARCH airfoil is characterized by a twofold increase in the drag coefficient during the airplane descent, compared with the airplane climb. A small bulge on the upper surface of the airfoil, formed at the place of thickening, leads to the formation of negative pressure.

The streamlined geometric shape of the Martin M 1 airfoil with a thickening in the middle ensures the formation of uniform negative pressure of the small value on the upper and lower surfaces in conditions of horizontal flight of the airplane. During maneuvers, the airplane wing is subjected to almost the same pressure values on the upper and lower surfaces, depending on the angle of attack.

The concave lower surface of the MATWIES6 airfoil forms the area of positive pressure during horizontal flight of the airplane. During the airplane climb, the camber of the airfoil increases the lifting force of the wing, and during the airplane descent, the pressure difference on the surfaces becomes minimal.

The MEG 64 airfoil, due to its specific geometric shape in the cross section, provides the formation of variable positive and negative pressures on edges and

surfaces at different angles of attack. The action of pressures of the small values on this airfoil is noted.

The barrel shape of the MH 27 airfoil, like the Martin M 1 airfoil, ensures the formation of low negative pressure on the surfaces at the angle of attack of 0 degrees. Maximum pressure is concentrated on the leading edge and part of the upper or lower surfaces mating with it during maneuvers.

The MILEY M06-13-128 airfoil, at the angle of attack of 15 degrees, experiences the greater drag than at the angle of attack of -15 degrees. Maximum negative pressure on the airfoil occurs during the airplane climb.

The MT722 airfoil is characterized by increasing the negative pressure value by two times on the leading edge during the airplane descent in the atmosphere. The low aerodynamic characteristics of the airplane wing are determined by the small pressure difference on the upper and lower surfaces.

Based on the calculated pressure contours obtained on the MVA-227 airfoil, the occurrence of the large lifting force due to the significant pressure difference on the wing surfaces is confirmed.

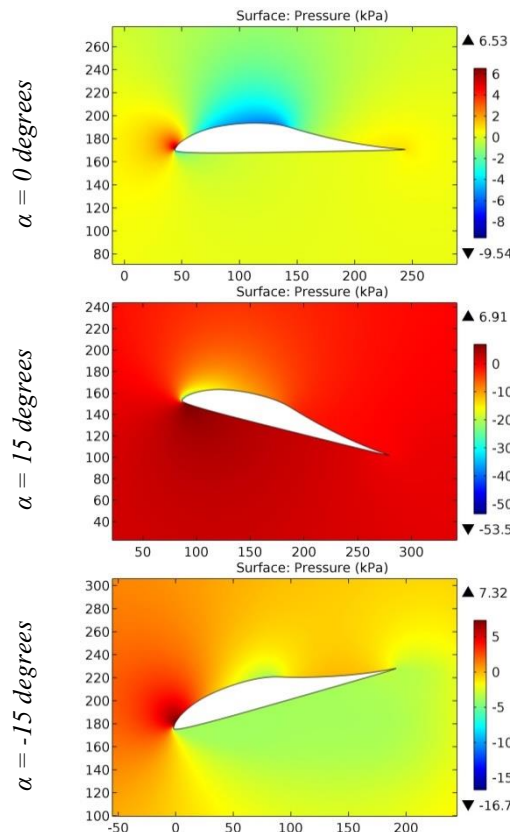


Figure 1. The pressure contours on the surfaces of the M06-13-1 airfoil.

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GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

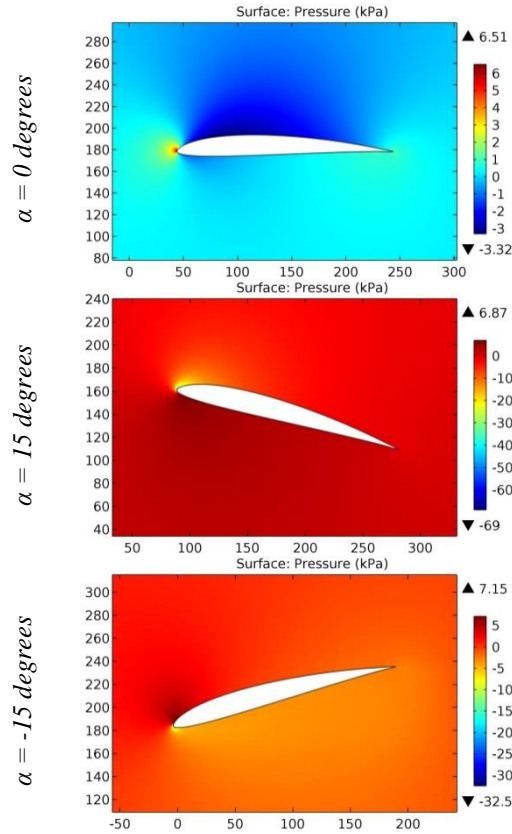


Figure 2. The pressure contours on the surfaces of the M3 - HB396 airfoil.

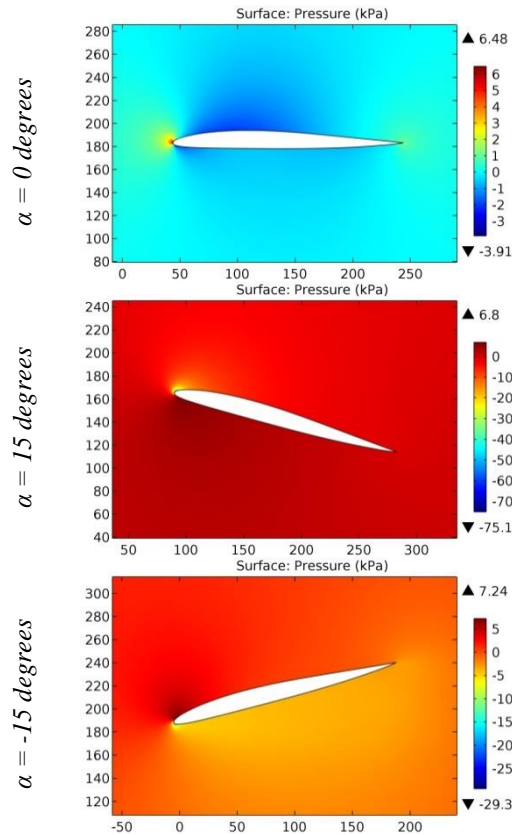


Figure 3. The pressure contours on the surfaces of the M6 (65%) airfoil.

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GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

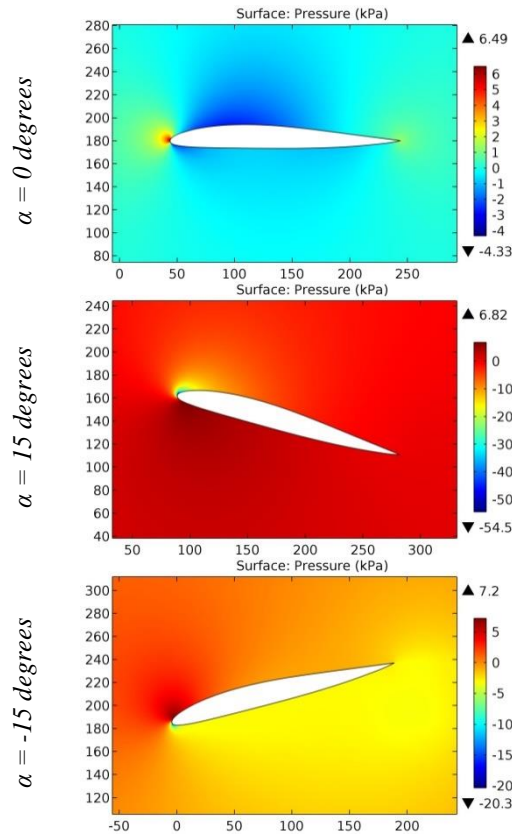


Figure 4. The pressure contours on the surfaces of the M6 (85%) airfoil.

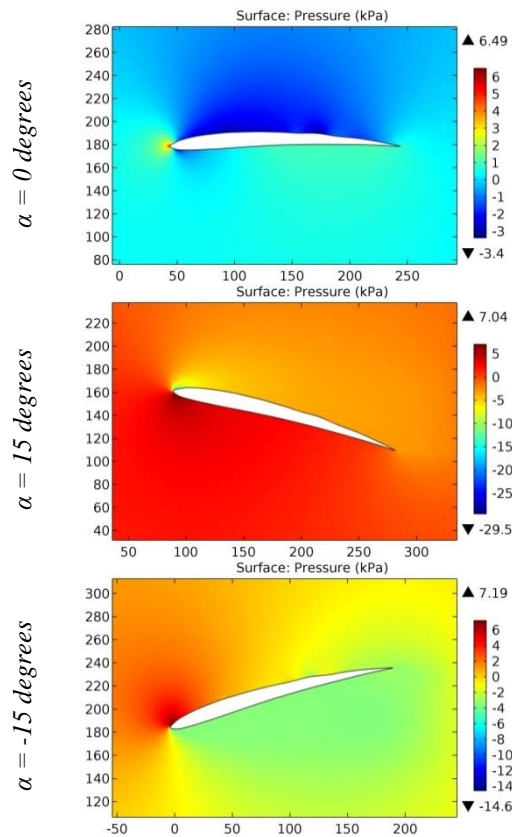


Figure 5. The pressure contours on the surfaces of the MA409 (original) airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

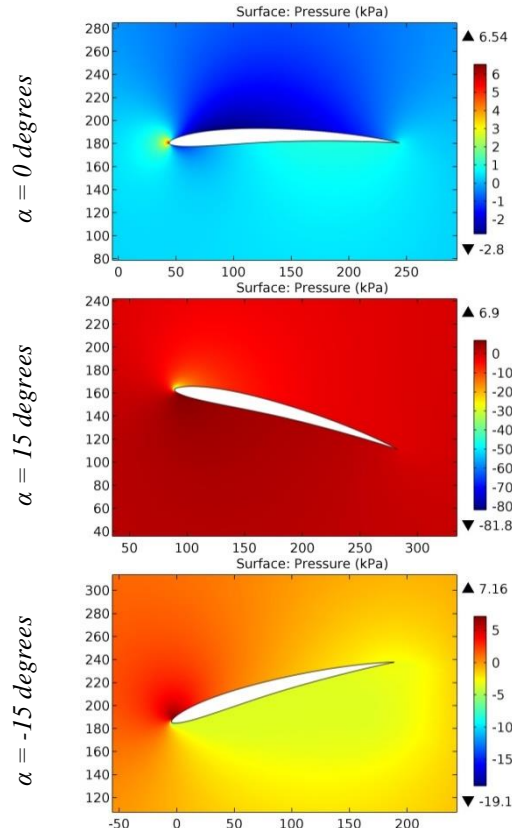


Figure 6. The pressure contours on the surfaces of the MA409 (smoothed) airfoil.

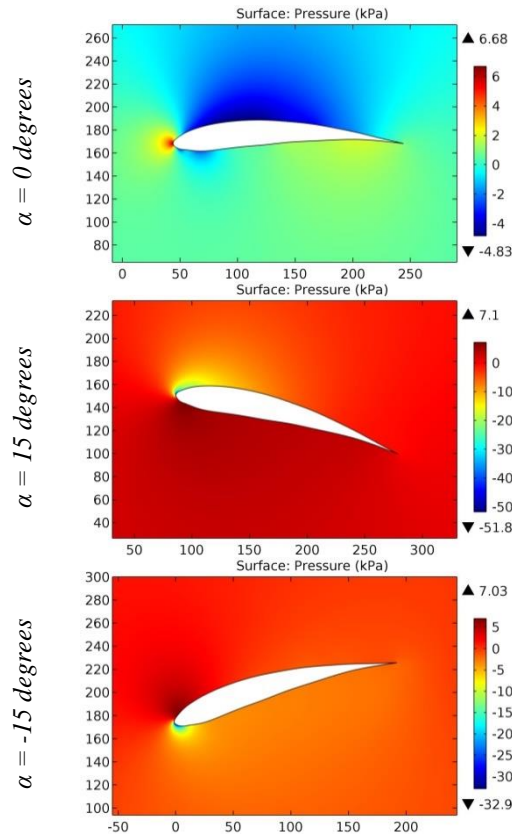


Figure 7. The pressure contours on the surfaces of the Marquardt airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

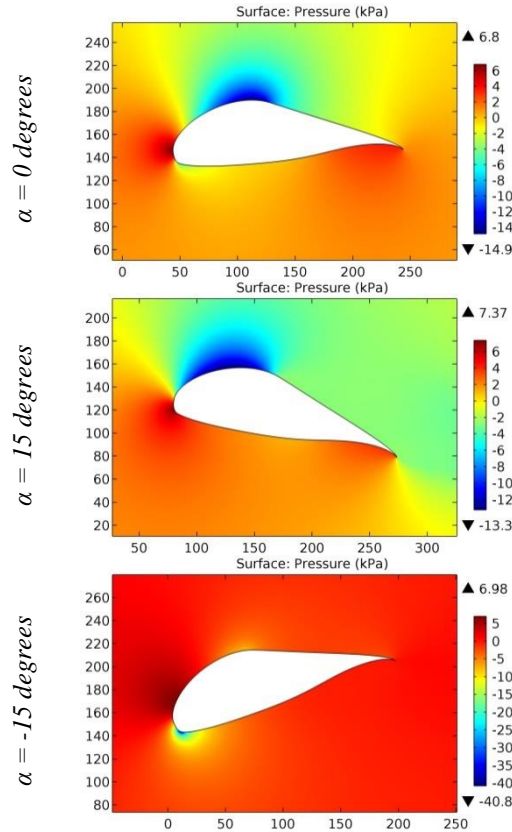


Figure 8. The pressure contours on the surfaces of the Marsden airfoil.

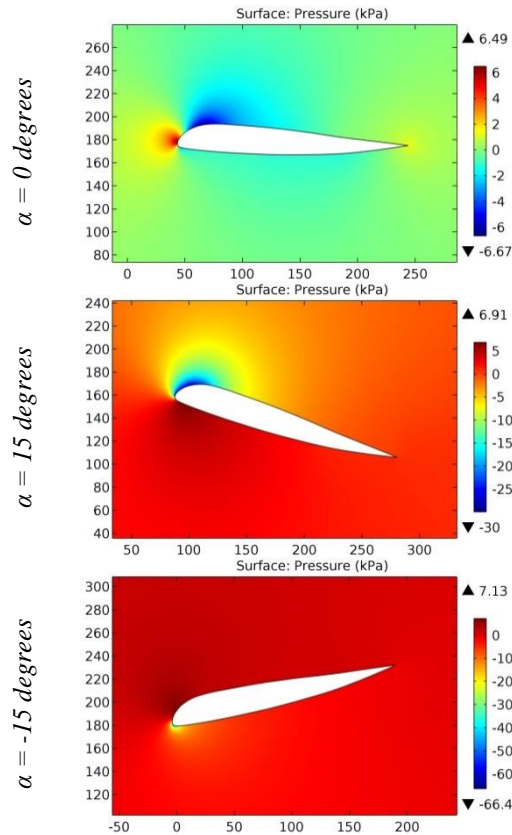


Figure 9. The pressure contours on the surfaces of the MARSKE MONARCH airfoil.

Impact Factor:

ISRA (India)	= 6.317	SIS (USA)	= 0.912	ICV (Poland)	= 6.630
ISI (Dubai, UAE)	= 1.582	ПИИЦ (Russia)	= 3.939	PIF (India)	= 1.940
GIF (Australia)	= 0.564	ESJI (KZ)	= 8.771	IBI (India)	= 4.260
JIF	= 1.500	SJIF (Morocco)	= 7.184	OAJI (USA)	= 0.350

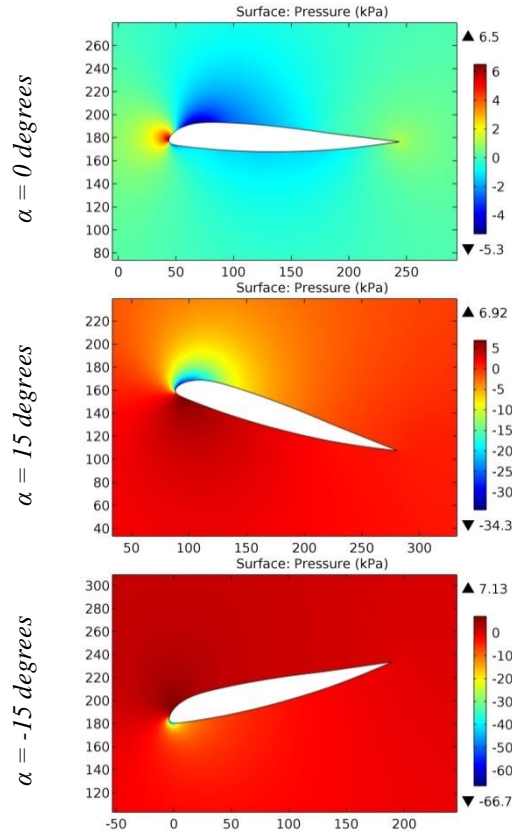


Figure 10. The pressure contours on the surfaces of the MARSKE PIONEER IA airfoil.

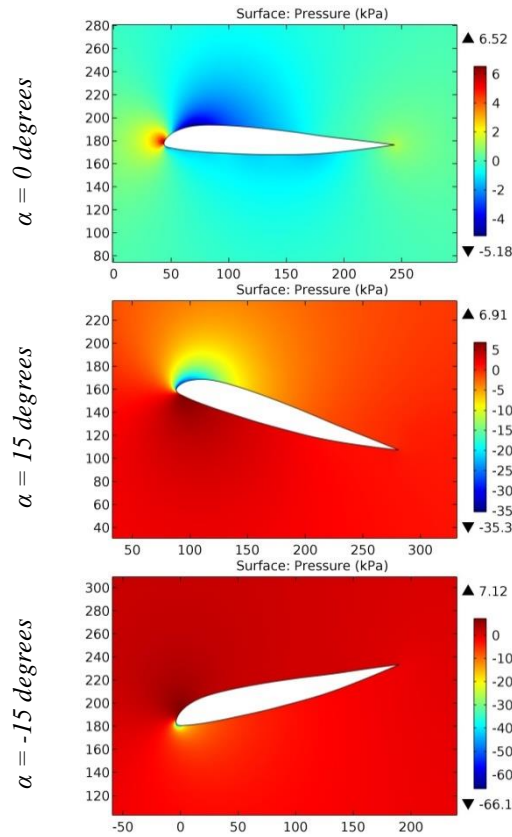


Figure 11. The pressure contours on the surfaces of the MARSKE PIONEER IID ROOT airfoil.

Impact Factor:

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GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

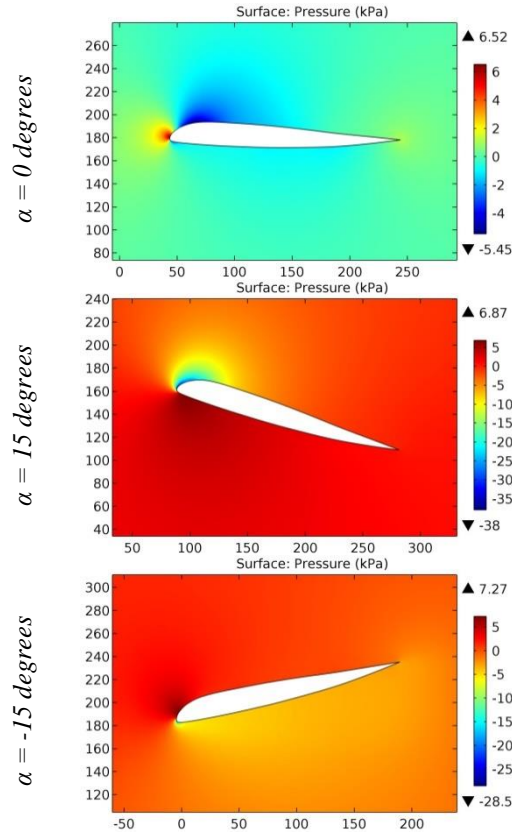


Figure 12. The pressure contours on the surfaces of the MARSKE PIONEER IID TIP airfoil.

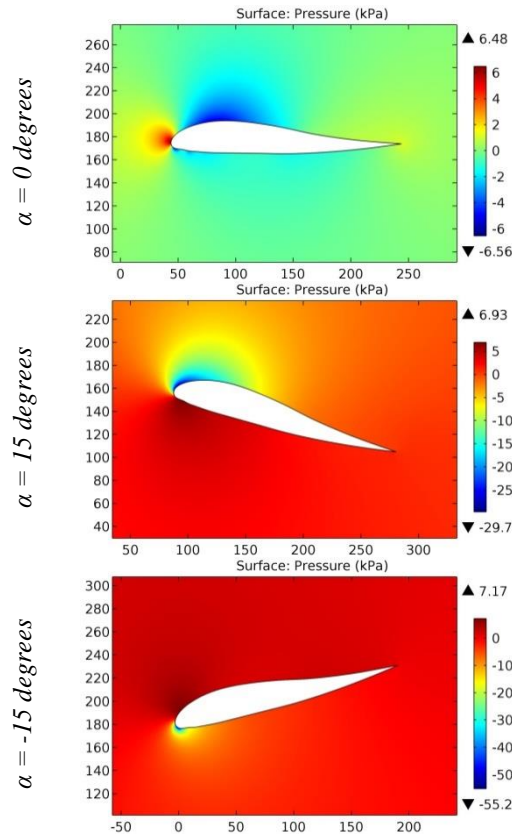


Figure 13. The pressure contours on the surfaces of the MARSKE XM-1D airfoil.

Impact Factor:

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GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

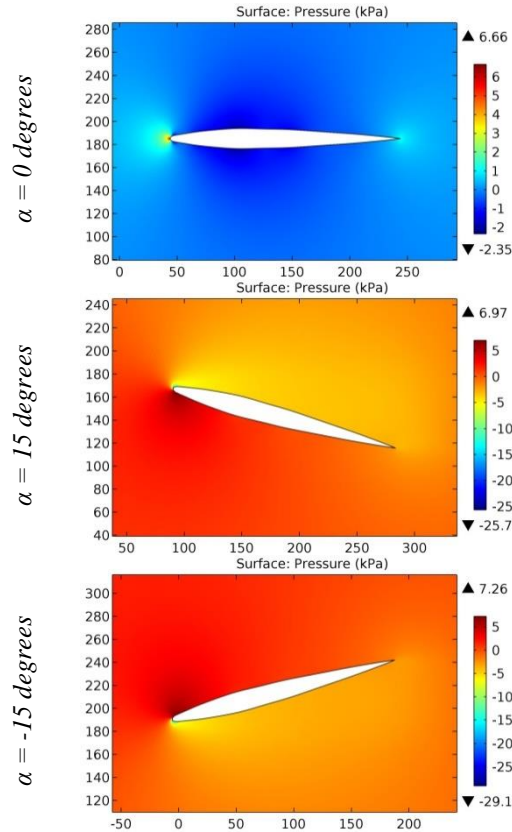


Figure 14. The pressure contours on the surfaces of the Martin M 1 airfoil.

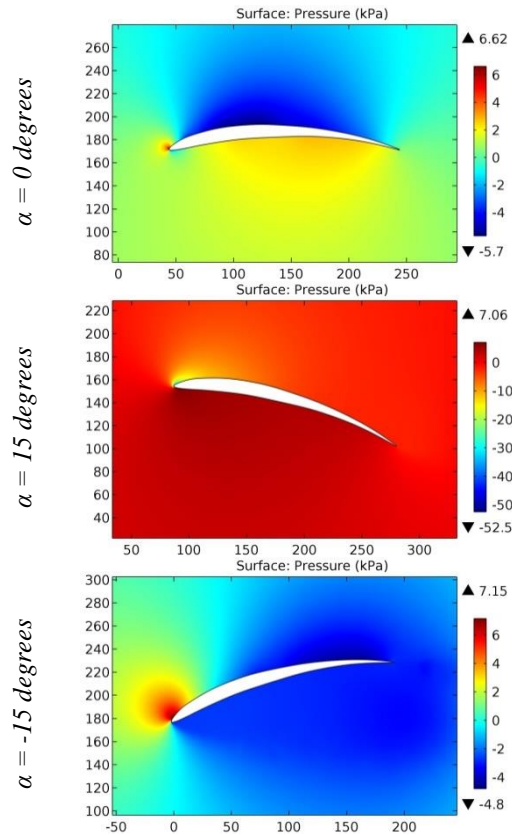


Figure 15. The pressure contours on the surfaces of the MATWIES6 airfoil.

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ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

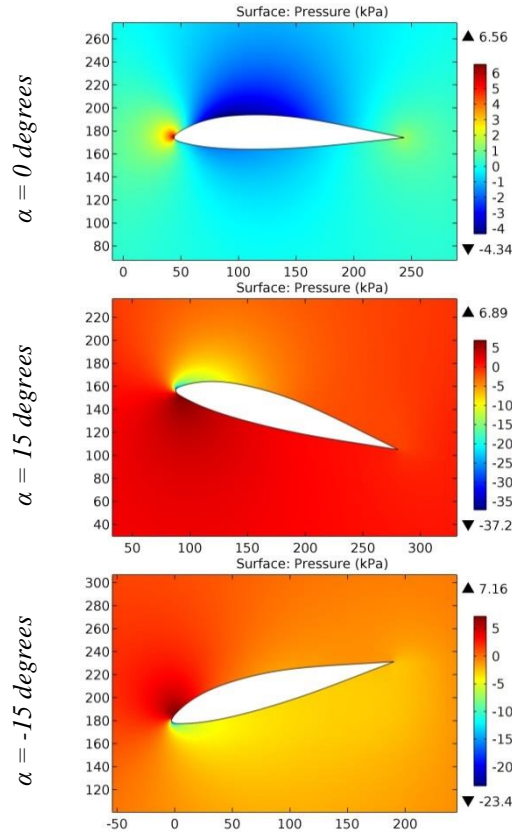


Figure 16. The pressure contours on the surfaces of the MB253515 airfoil.

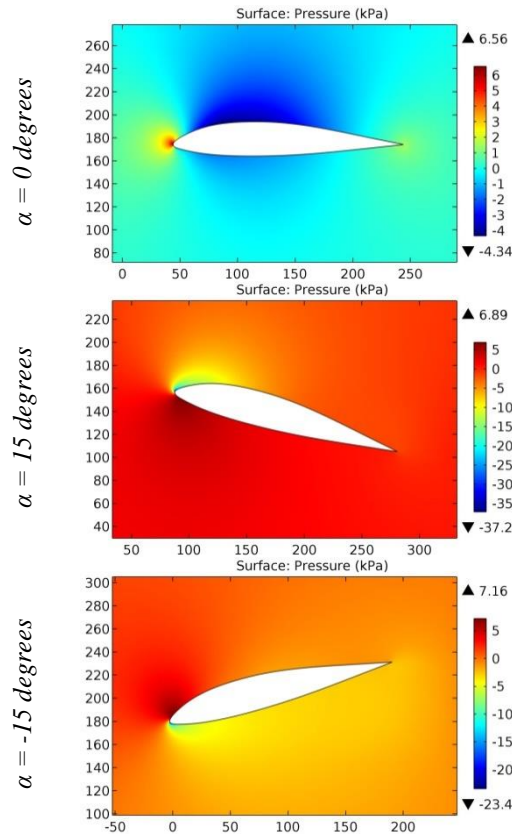


Figure 17. The pressure contours on the surfaces of the MB253515 15,0% smoothed airfoil.

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ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

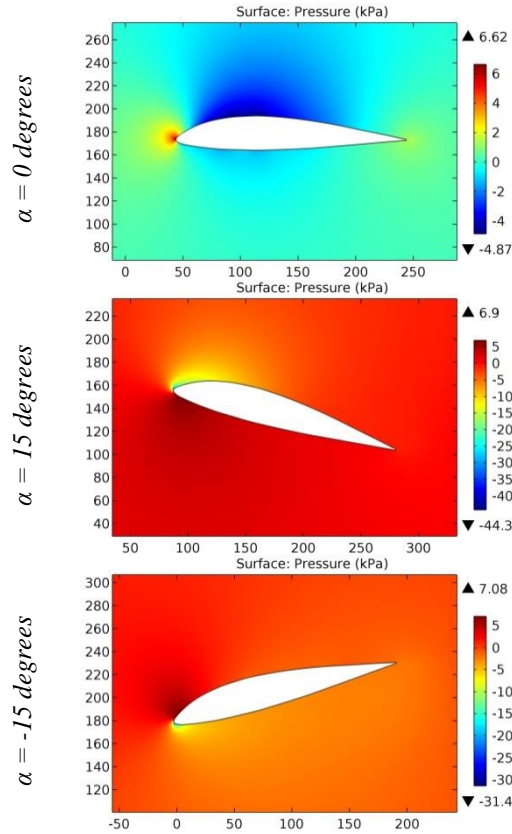


Figure 18. The pressure contours on the surfaces of the MB303515 airfoil.

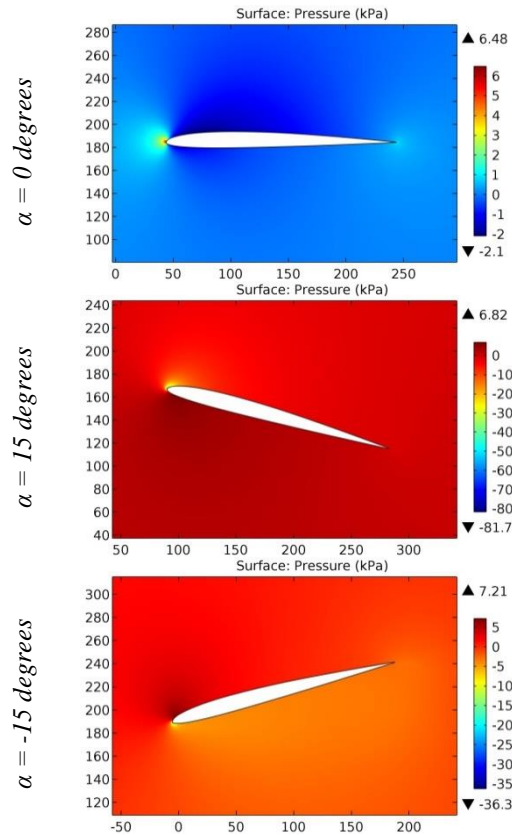


Figure 19. The pressure contours on the surfaces of the mb7136 airfoil.

Impact Factor:

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ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

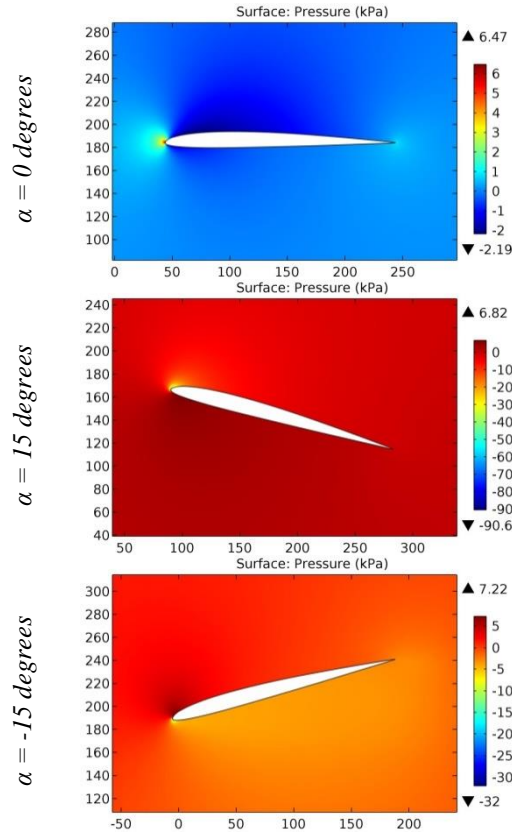


Figure 20. The pressure contours on the surfaces of the mb714 airfoil.

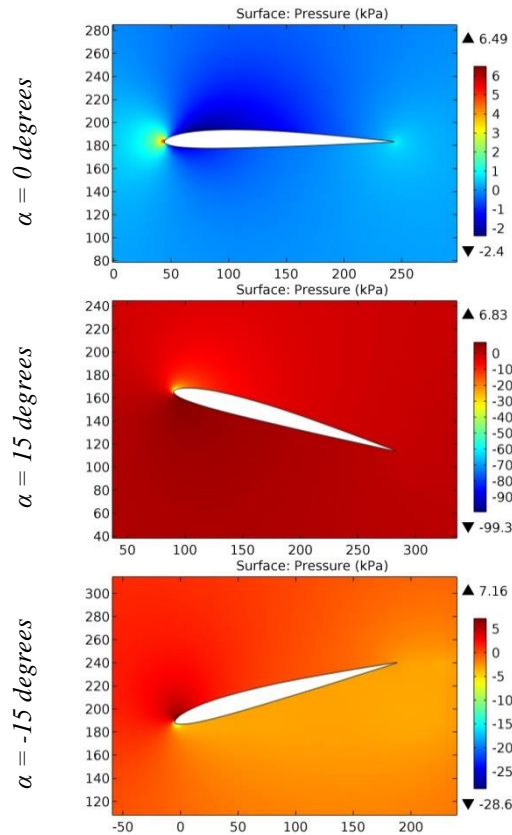


Figure 21. The pressure contours on the surfaces of the mc813 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

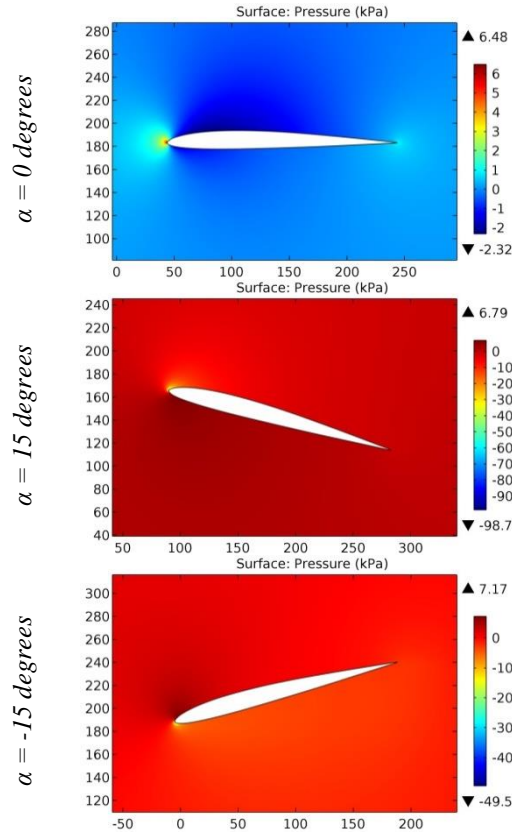


Figure 22. The pressure contours on the surfaces of the md8135 airfoil.

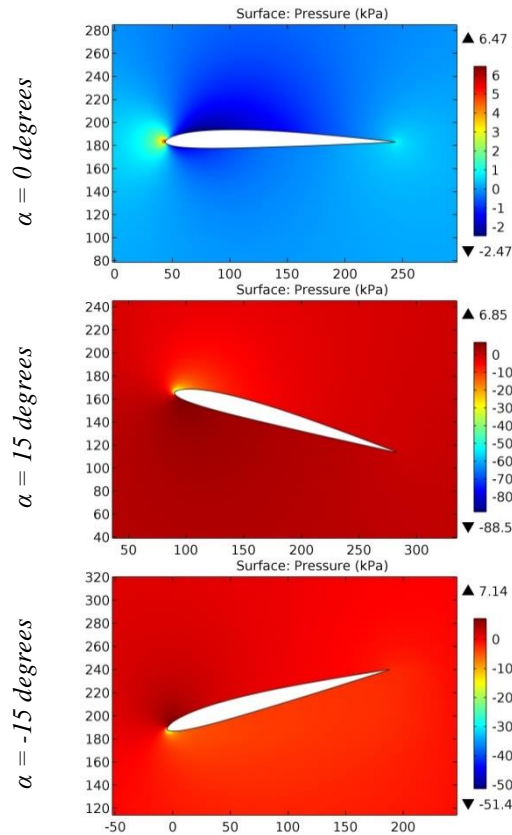


Figure 23. The pressure contours on the surfaces of the md814 airfoil.

Impact Factor:

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ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

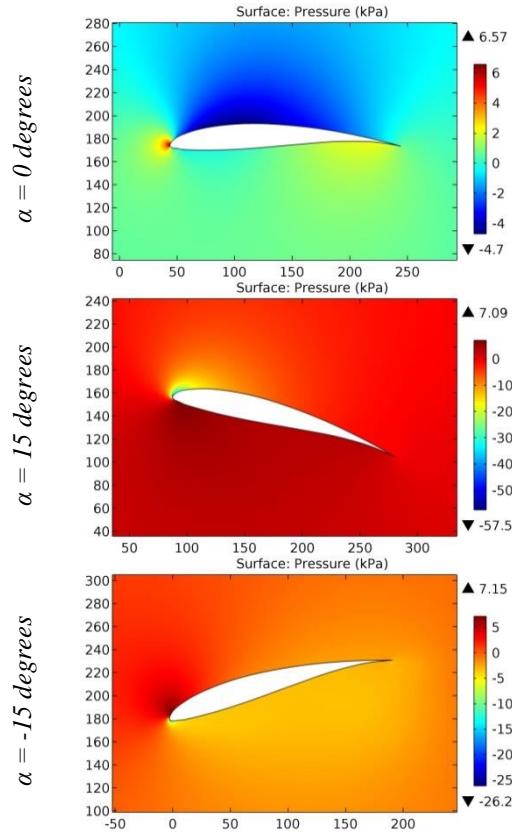


Figure 24. The pressure contours on the surfaces of the MEG 59 airfoil.

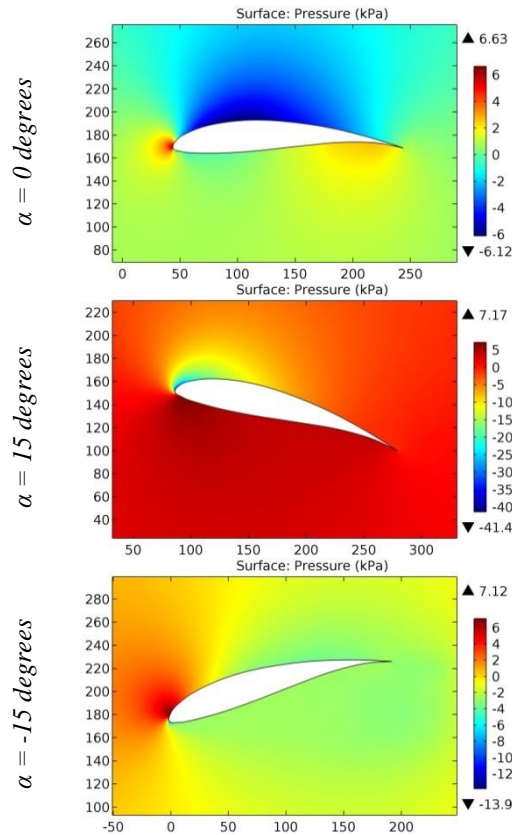


Figure 25. The pressure contours on the surfaces of the MEG 62-63137 airfoil.

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GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

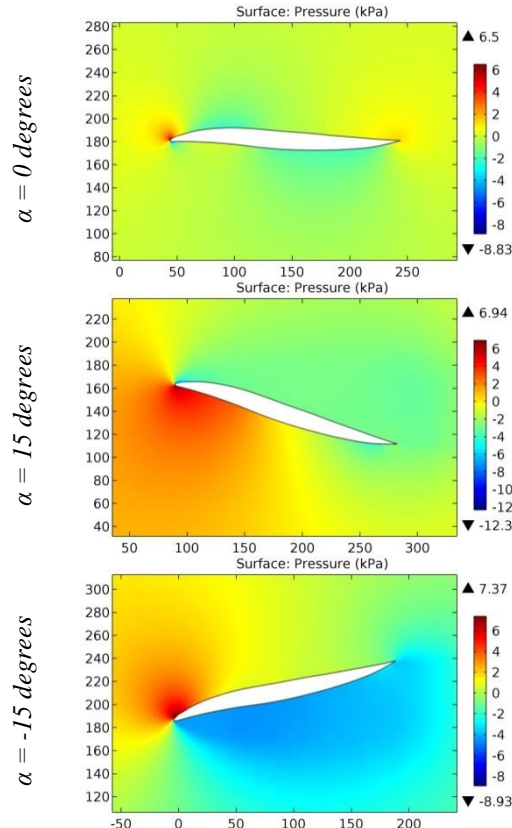


Figure 26. The pressure contours on the surfaces of the MEG 64 airfoil.

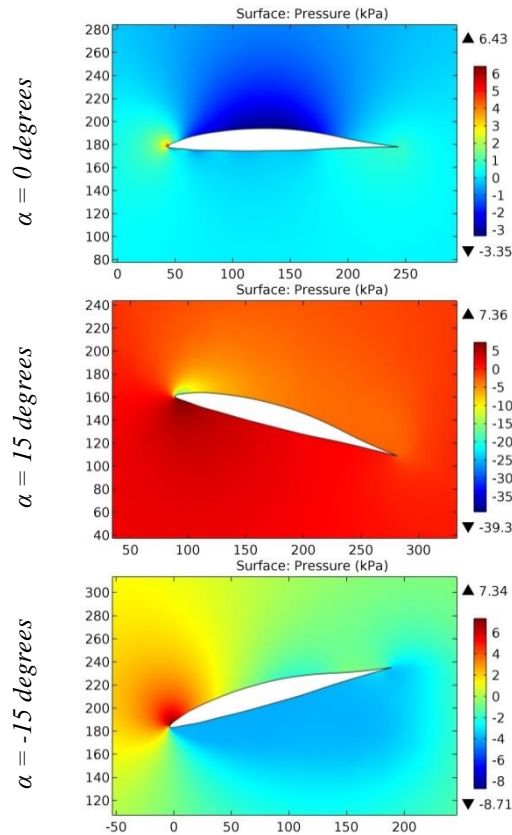


Figure 27. The pressure contours on the surfaces of the MEG 66 airfoil.

Impact Factor:

SIS (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
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GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

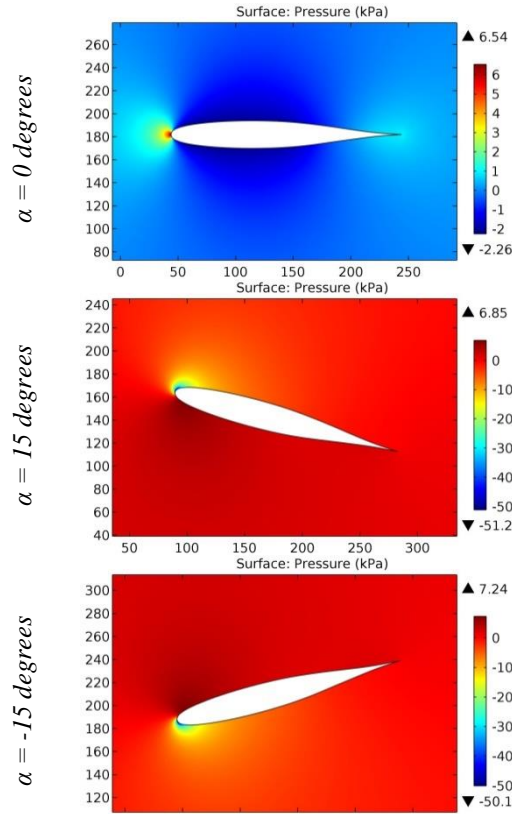


Figure 28. The pressure contours on the surfaces of the MEG 69-012 airfoil.

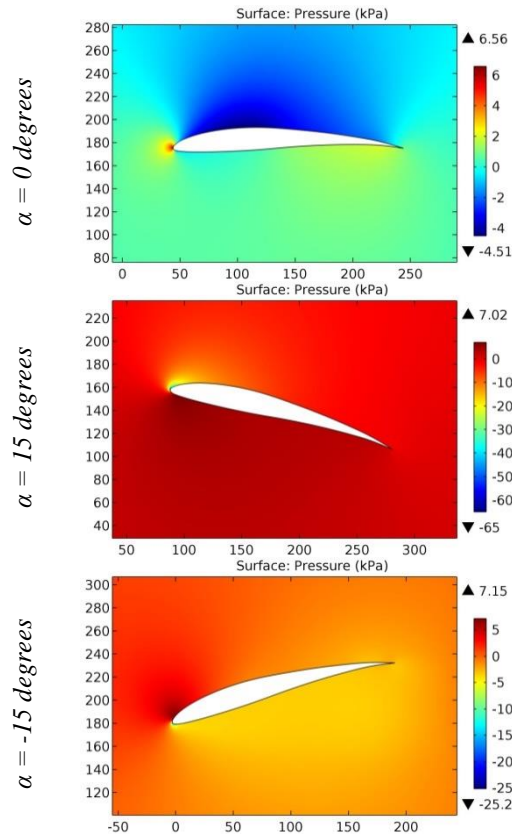


Figure 29. The pressure contours on the surfaces of the MEG-197 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

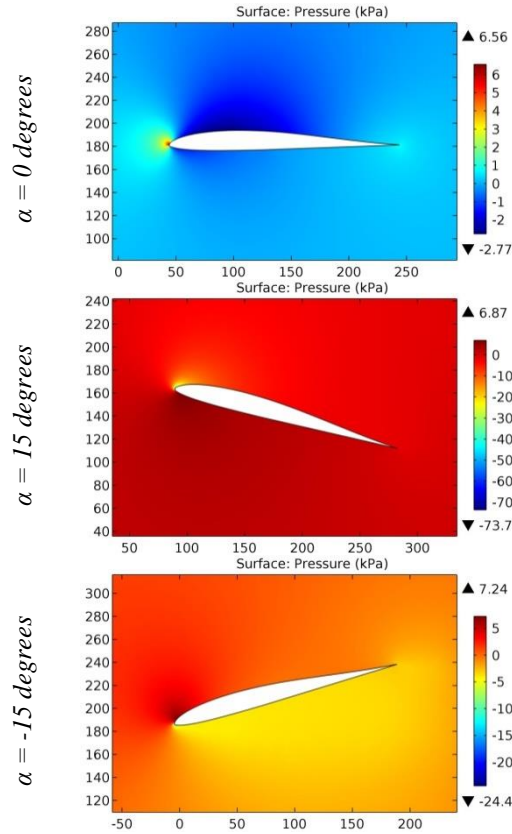


Figure 30. The pressure contours on the surfaces of the MG 08 airfoil.

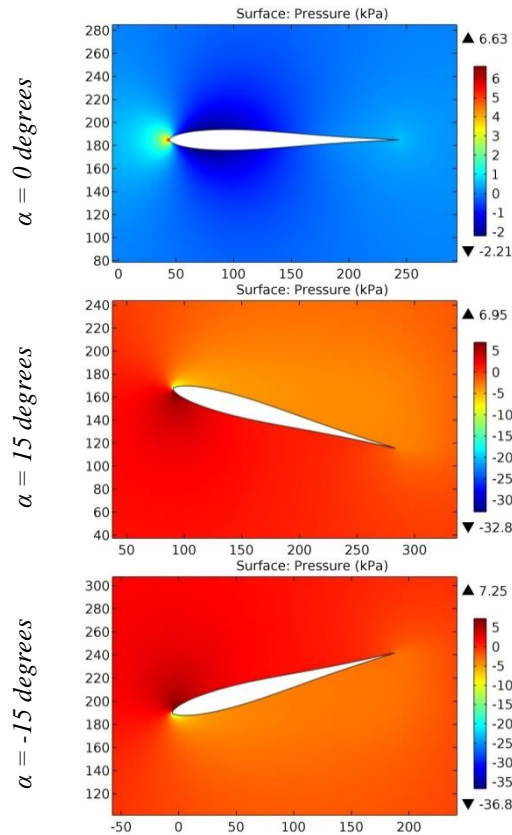


Figure 31. The pressure contours on the surfaces of the MG05 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

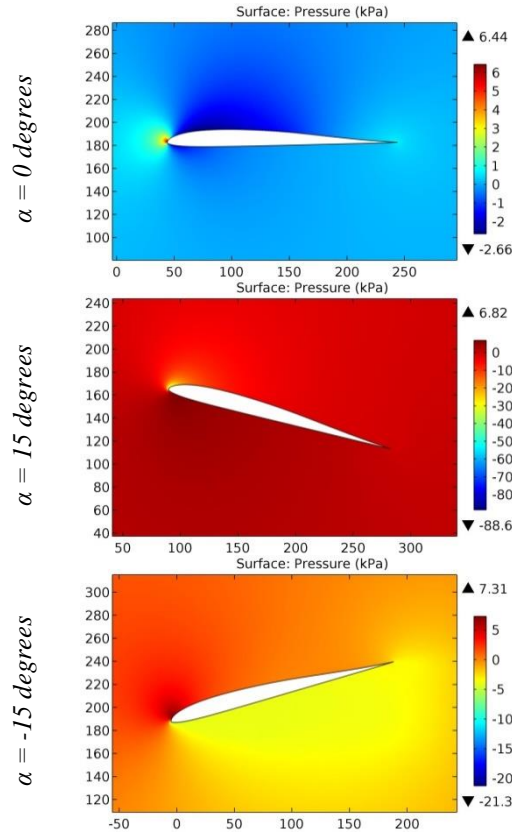


Figure 32. The pressure contours on the surfaces of the MG06 airfoil.

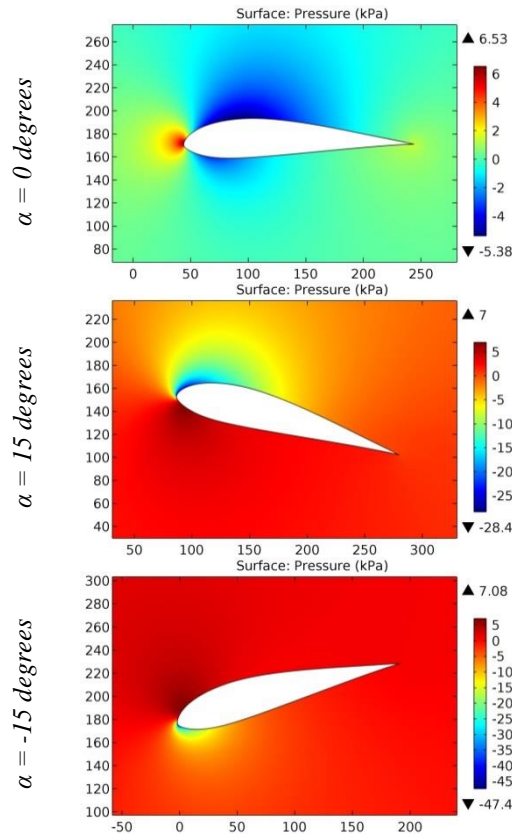


Figure 33. The pressure contours on the surfaces of the MH 102 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

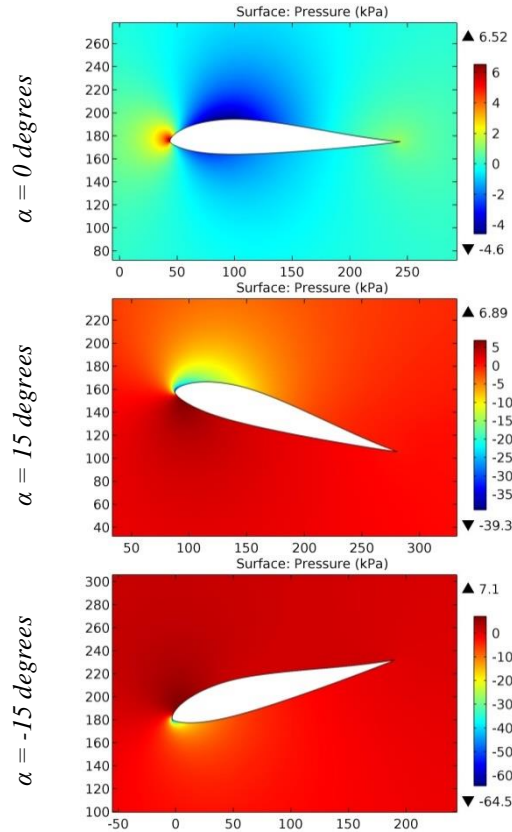


Figure 34. The pressure contours on the surfaces of the MH 104 airfoil.

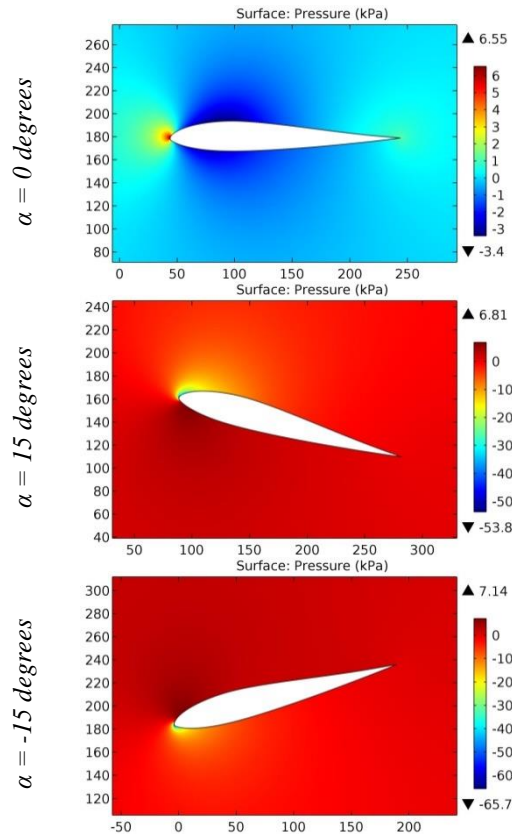


Figure 35. The pressure contours on the surfaces of the MH 106 airfoil.

Impact Factor:

SISRA (India)	= 6.317	SIS (USA)	= 0.912	ICV (Poland)	= 6.630
ISI (Dubai, UAE)	= 1.582	ПИИЦ (Russia)	= 3.939	PIF (India)	= 1.940
GIF (Australia)	= 0.564	ESJI (KZ)	= 8.771	IBI (India)	= 4.260
JIF	= 1.500	SJIF (Morocco)	= 7.184	OAJI (USA)	= 0.350

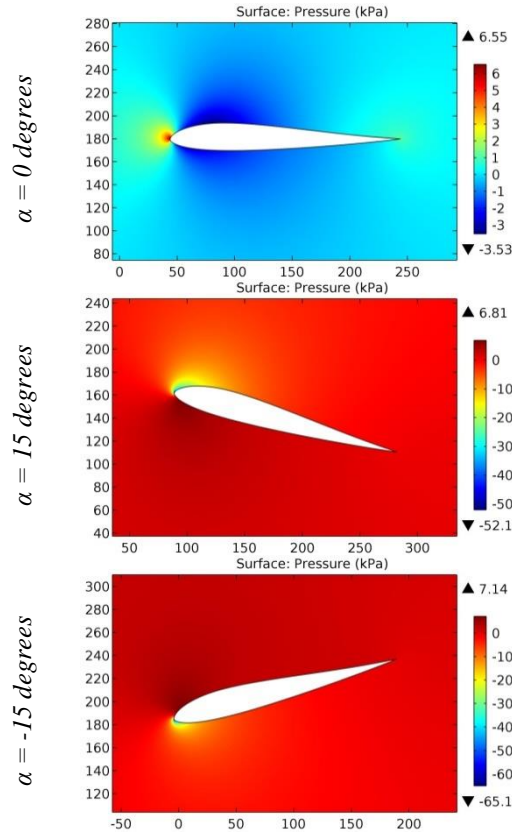


Figure 36. The pressure contours on the surfaces of the MH 108 airfoil.

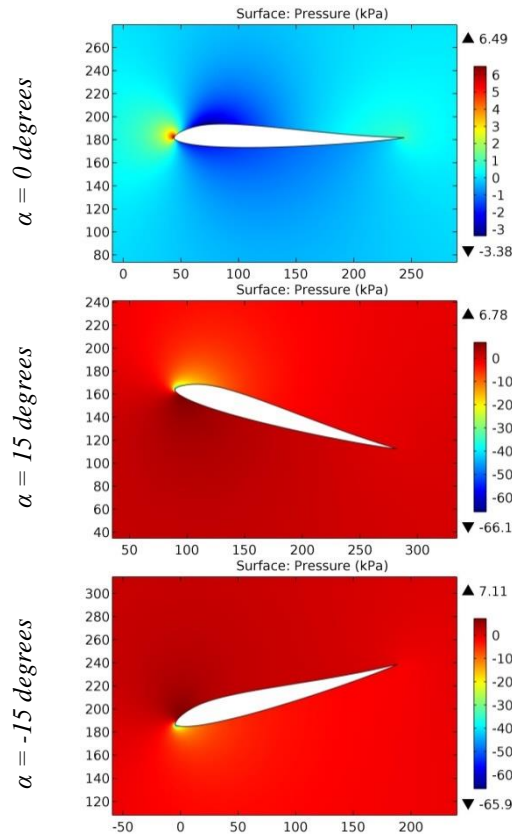


Figure 37. The pressure contours on the surfaces of the MH 110 airfoil.

Impact Factor:

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ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

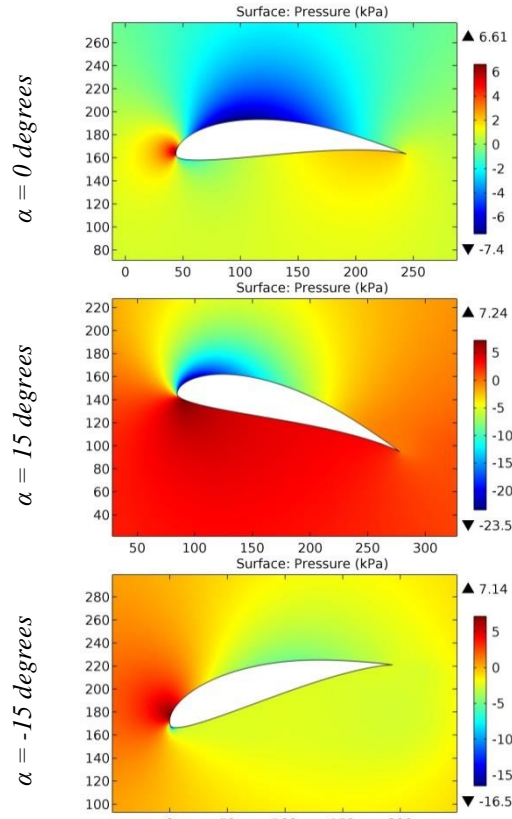


Figure 38. The pressure contours on the surfaces of the MH 112 airfoil.

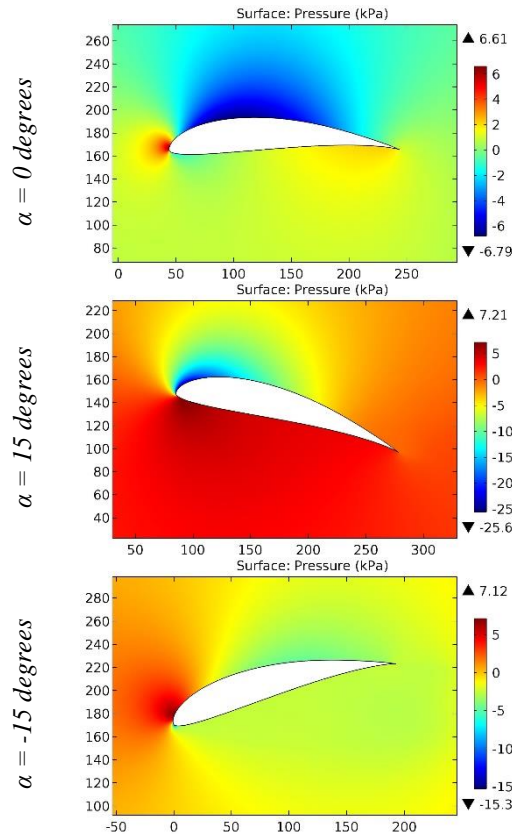


Figure 39. The pressure contours on the surfaces of the MH 113 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

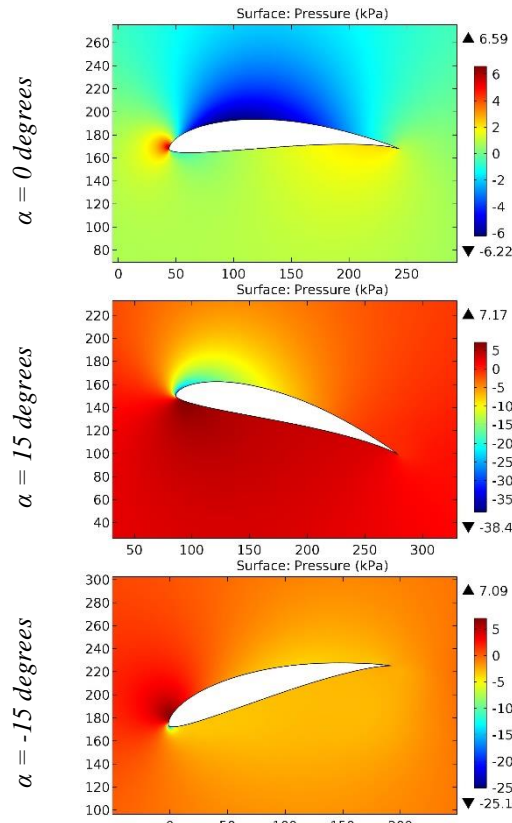


Figure 40. The pressure contours on the surfaces of the MH 114 airfoil.

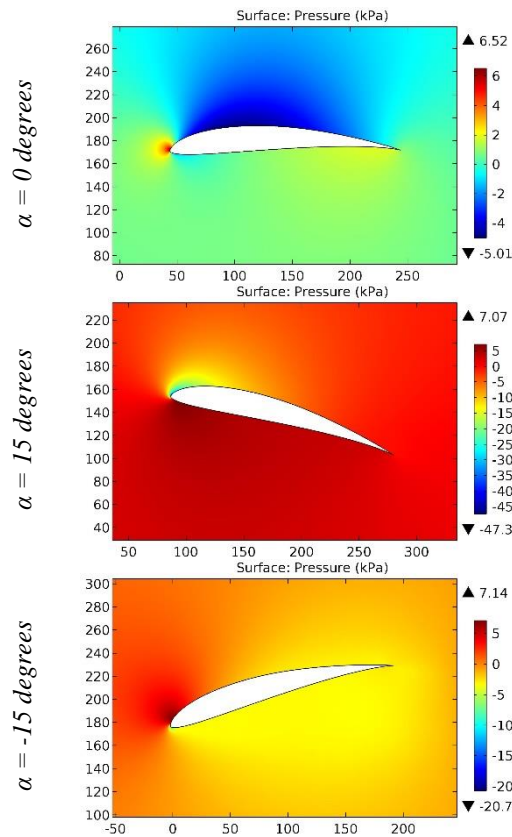


Figure 41. The pressure contours on the surfaces of the MH 115 airfoil.

Impact Factor:

SISRA (India)	= 6.317	SIS (USA)	= 0.912	ICV (Poland)	= 6.630
ISI (Dubai, UAE)	= 1.582	ПИИЦ (Russia)	= 3.939	PIF (India)	= 1.940
GIF (Australia)	= 0.564	ESJI (KZ)	= 8.771	IBI (India)	= 4.260
JIF	= 1.500	SJIF (Morocco)	= 7.184	OAJI (USA)	= 0.350

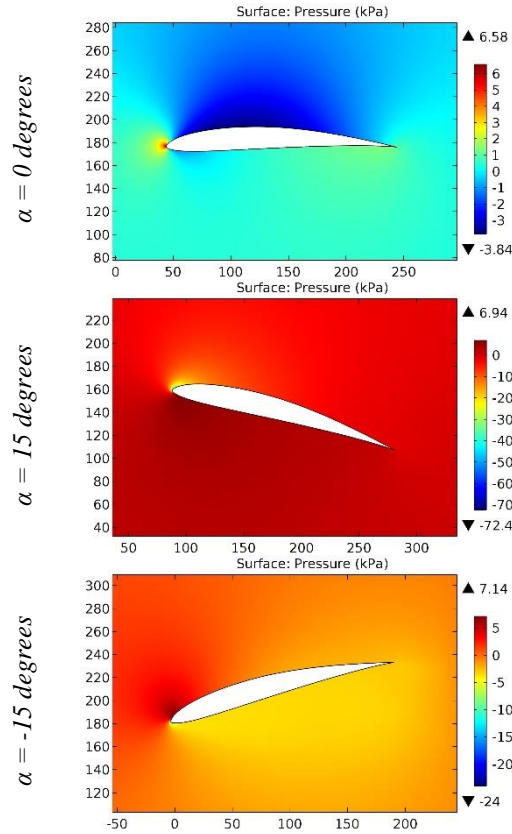


Figure 42. The pressure contours on the surfaces of the MH 116 airfoil.

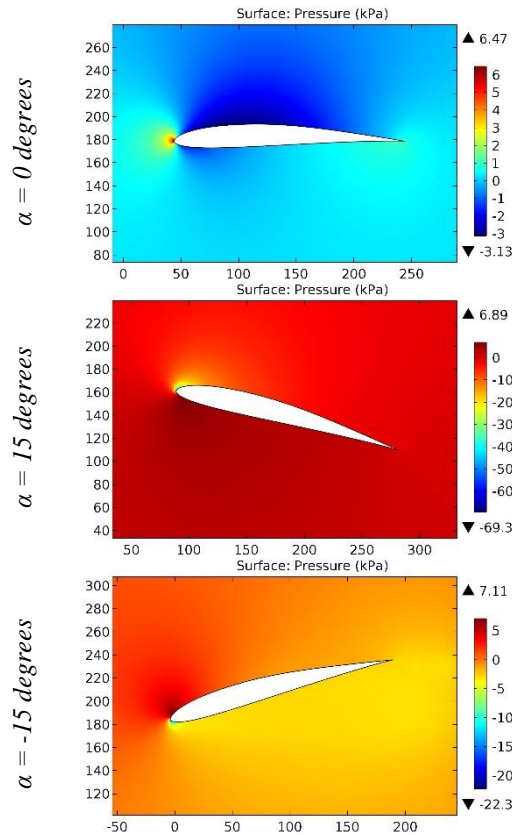


Figure 43. The pressure contours on the surfaces of the MH 117 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

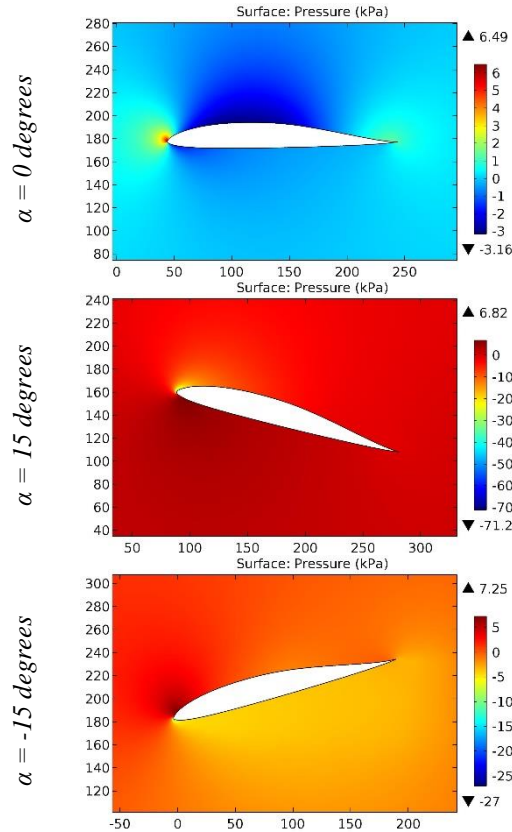


Figure 44. The pressure contours on the surfaces of the MH 18 airfoil.

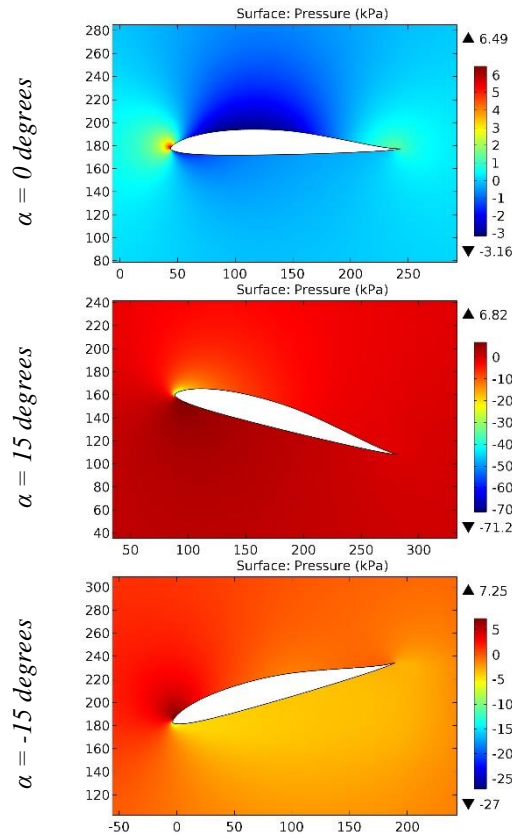


Figure 45. The pressure contours on the surfaces of the MH 18 11,14% airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

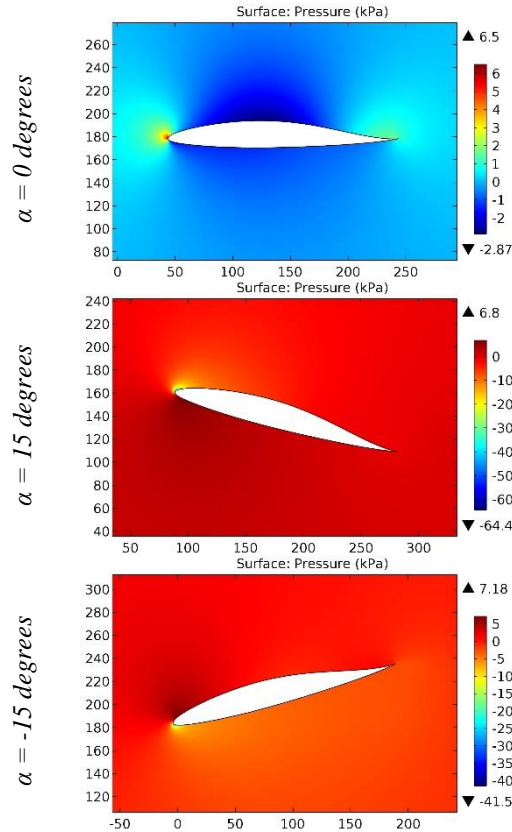


Figure 46. The pressure contours on the surfaces of the MH 18B airfoil.

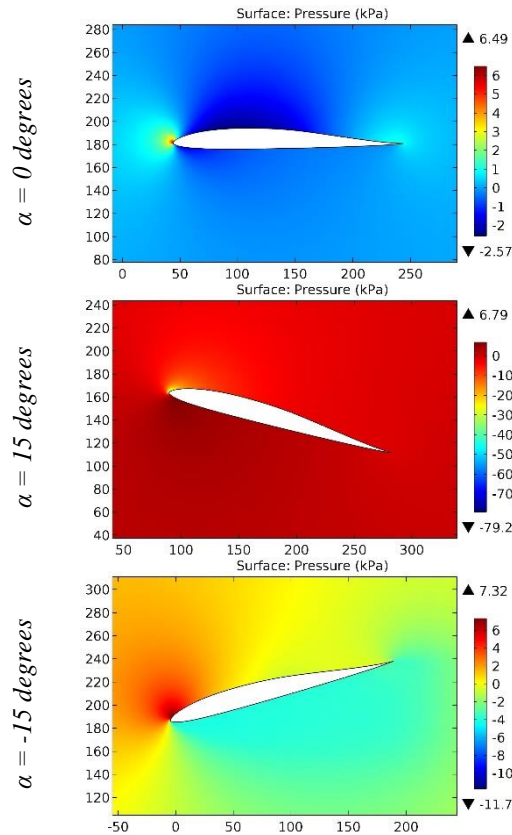


Figure 47. The pressure contours on the surfaces of the MH 20 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

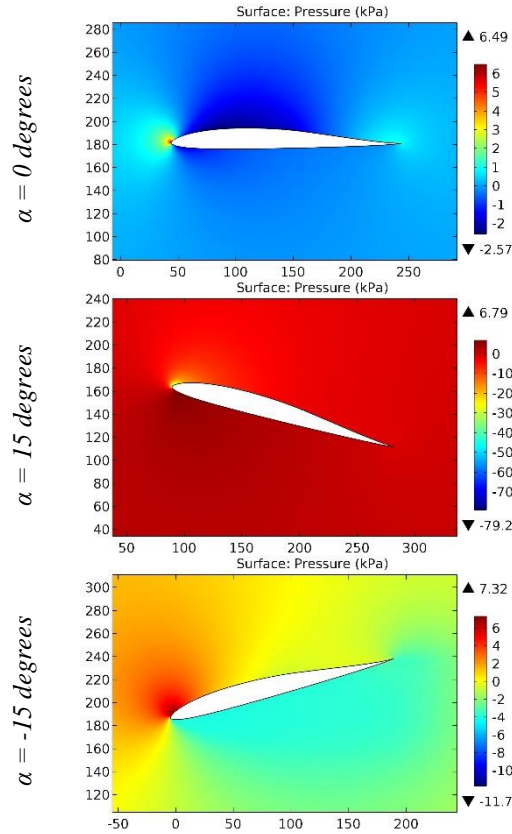


Figure 48. The pressure contours on the surfaces of the MH 20 9,02% airfoil.

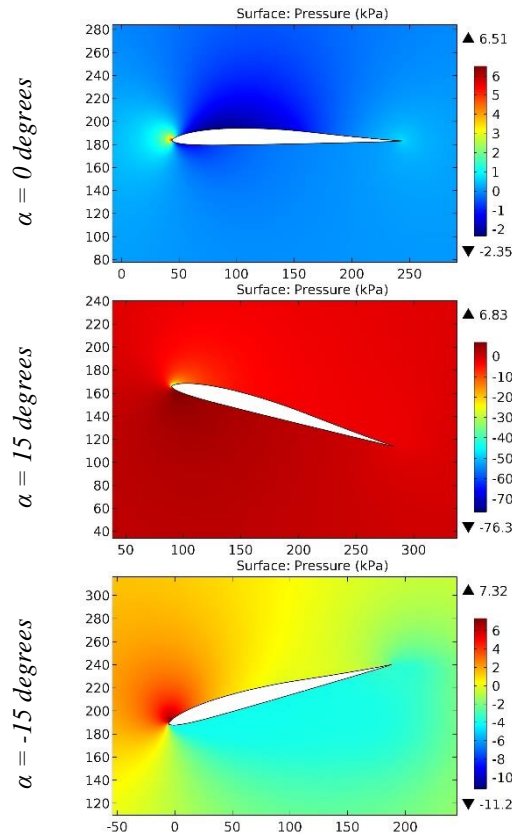


Figure 49. The pressure contours on the surfaces of the MH 22 airfoil.

Impact Factor:

SISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

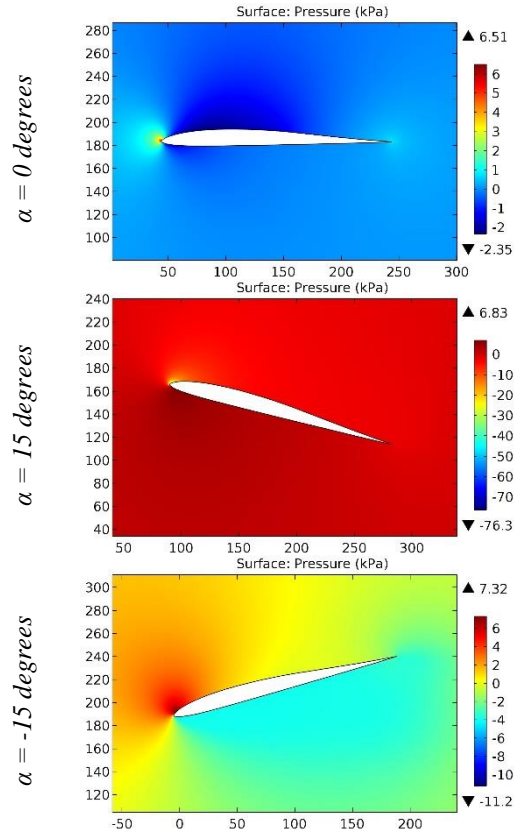


Figure 50. The pressure contours on the surfaces of the MH 22 7,21% airfoil.

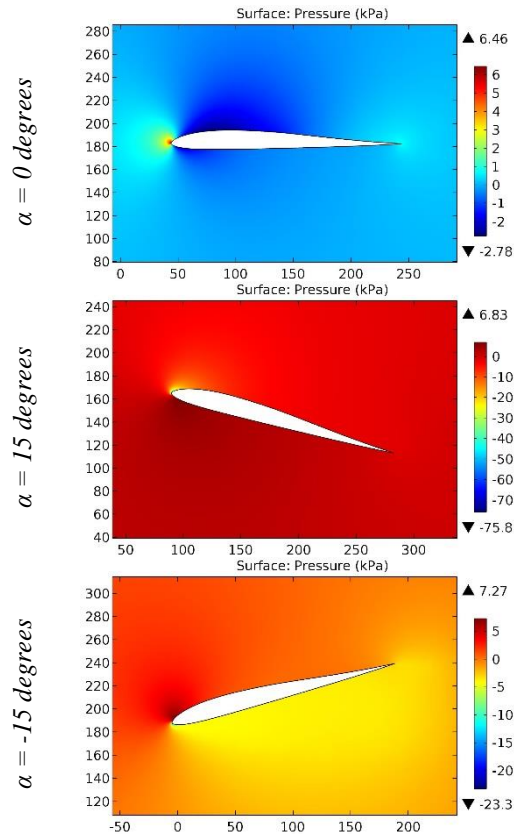


Figure 51. The pressure contours on the surfaces of the MH 22-Mod,3 airfoil.

Impact Factor:

SISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

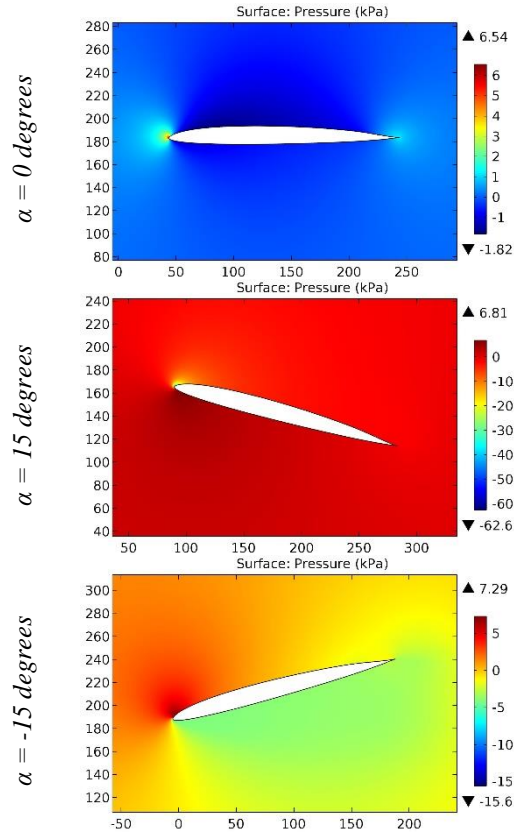


Figure 52. The pressure contours on the surfaces of the MH 23 airfoil.

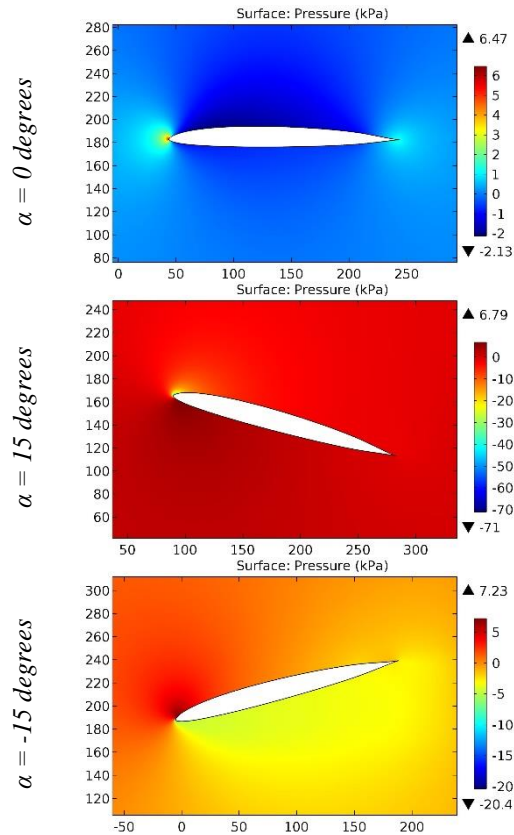


Figure 53. The pressure contours on the surfaces of the MH 24 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

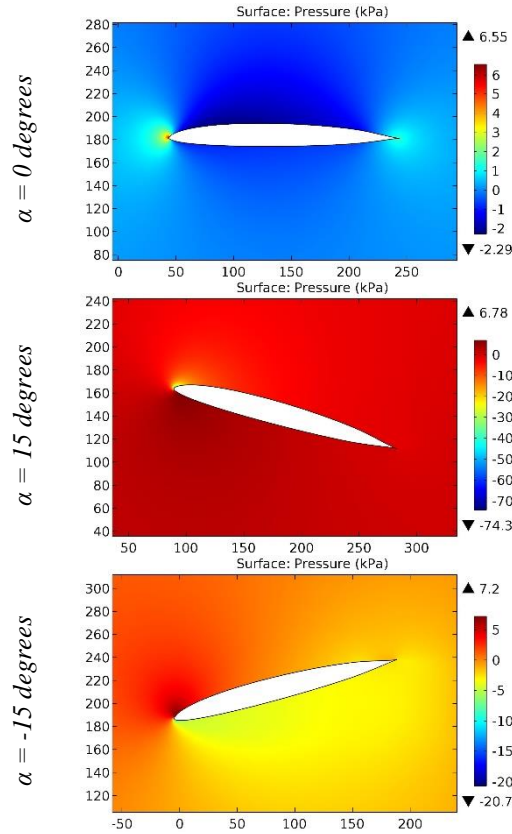


Figure 54. The pressure contours on the surfaces of the MH 25 airfoil.

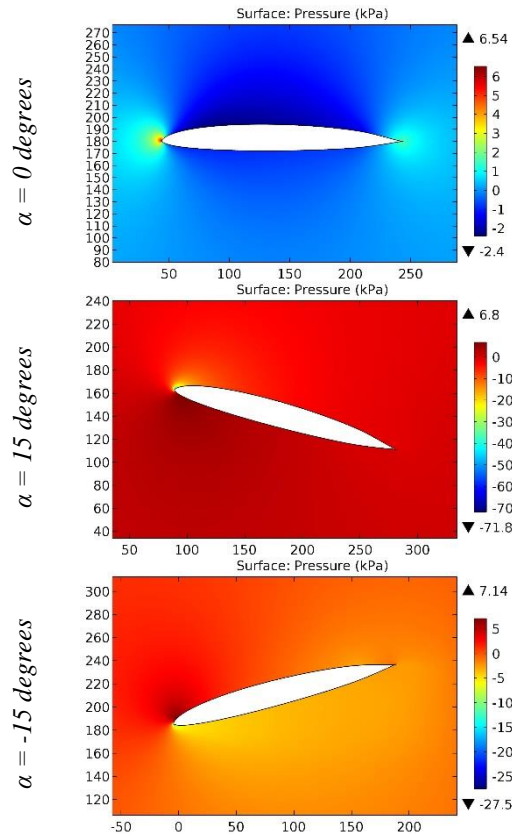


Figure 55. The pressure contours on the surfaces of the MH 26 airfoil.

Impact Factor:

SISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

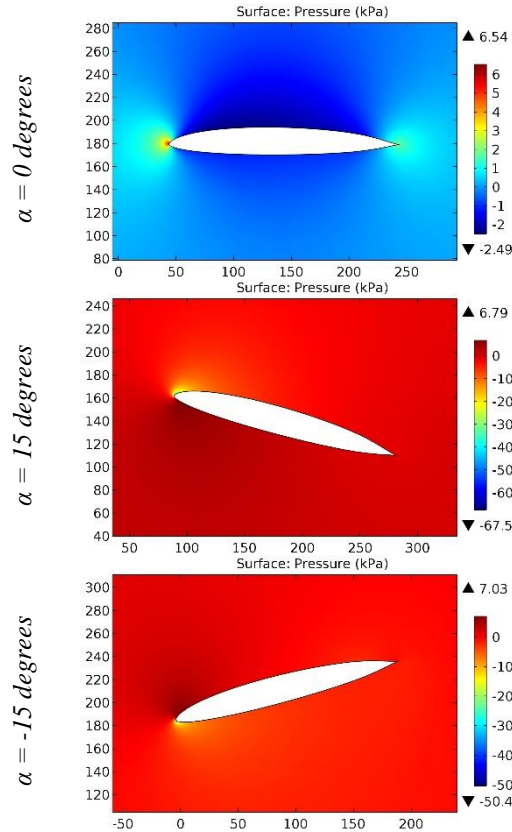


Figure 56. The pressure contours on the surfaces of the MH 27 airfoil.

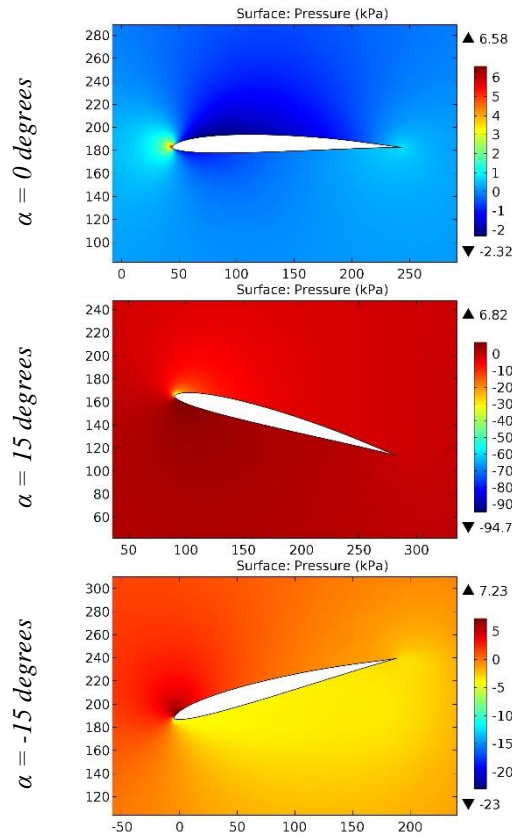


Figure 57. The pressure contours on the surfaces of the MH 30 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

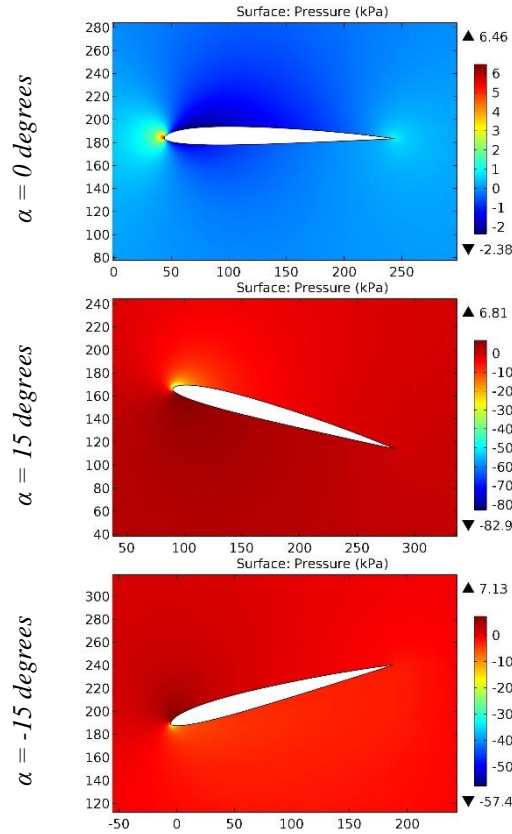


Figure 58. The pressure contours on the surfaces of the MH 31 airfoil.

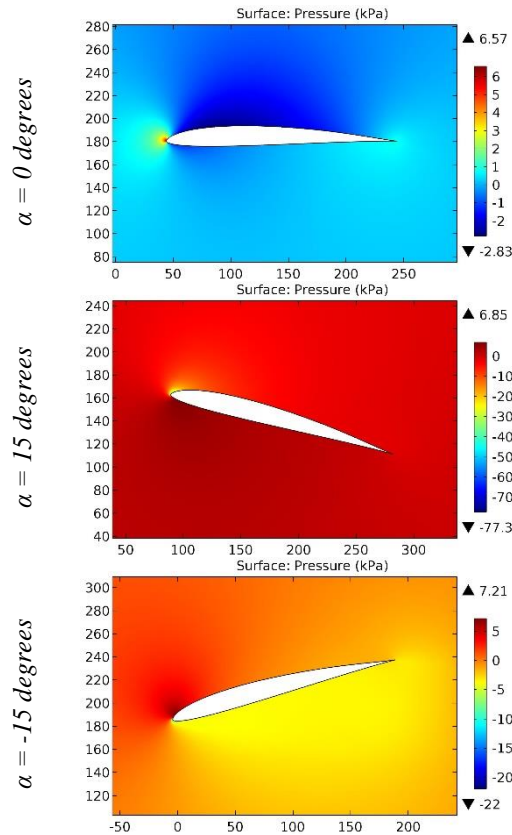


Figure 59. The pressure contours on the surfaces of the MH 32 airfoil.

Impact Factor:

SISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

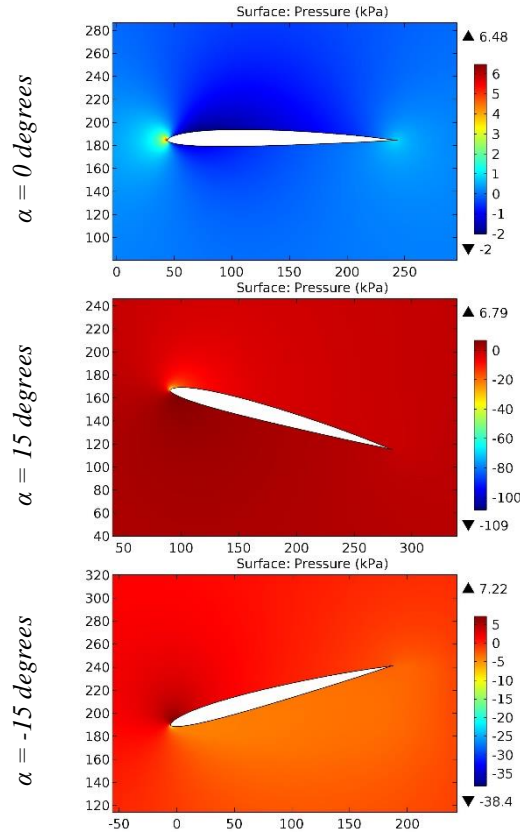


Figure 60. The pressure contours on the surfaces of the MH 33 airfoil.

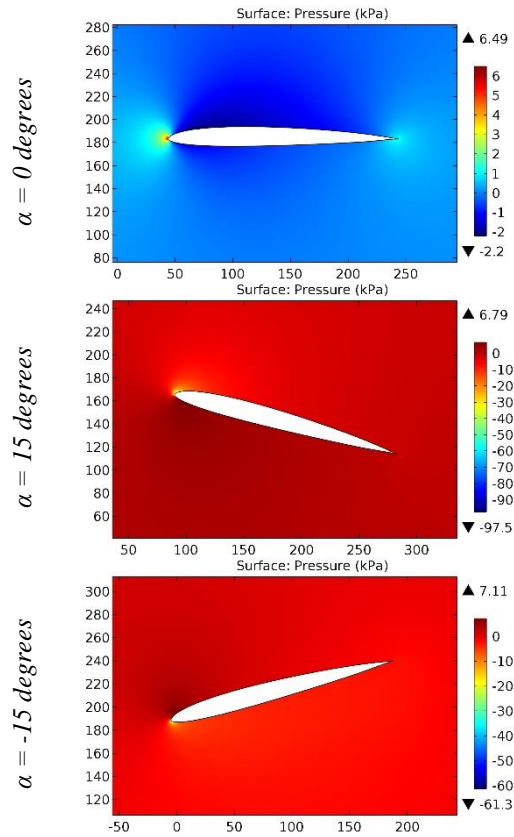


Figure 61. The pressure contours on the surfaces of the MH 34 airfoil.

Impact Factor:

SISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

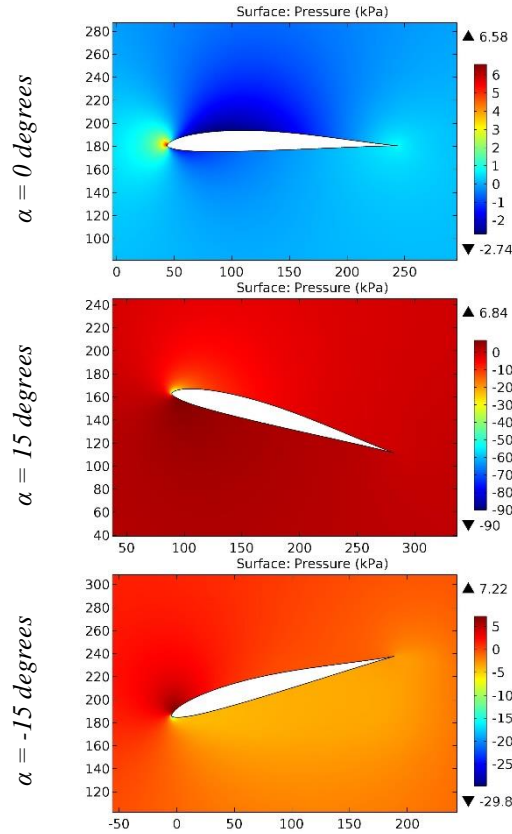


Figure 62. The pressure contours on the surfaces of the MH 42 airfoil.

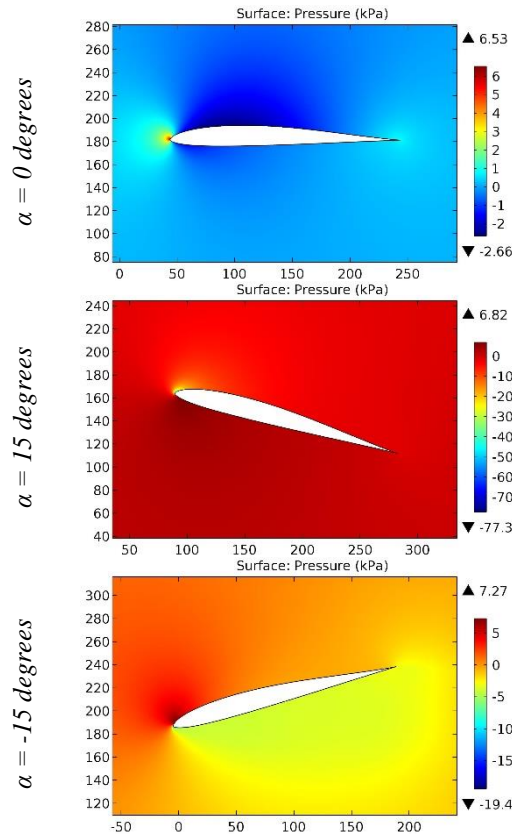


Figure 63. The pressure contours on the surfaces of the MH 42 8,94% airfoil.

Impact Factor:

SISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

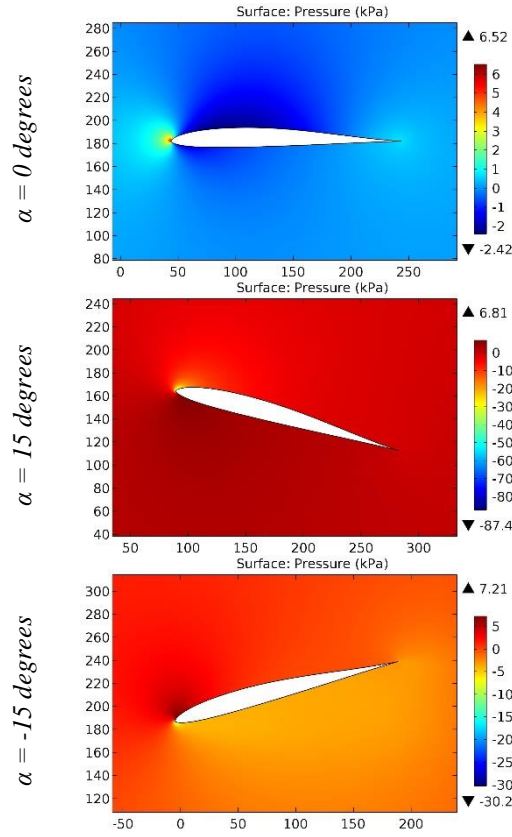


Figure 64. The pressure contours on the surfaces of the MH 43 airfoil.

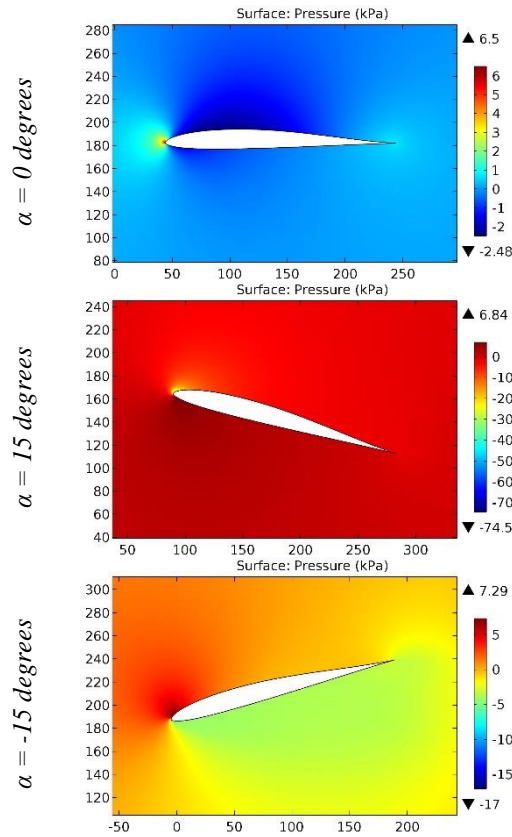


Figure 65. The pressure contours on the surfaces of the MH 43 8,5% airfoil.

Impact Factor:

SISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

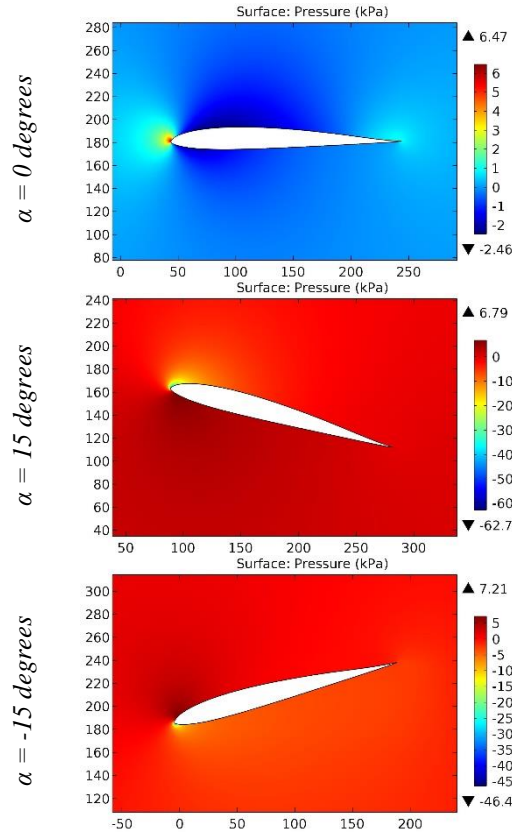


Figure 66. The pressure contours on the surfaces of the MH 44 airfoil.

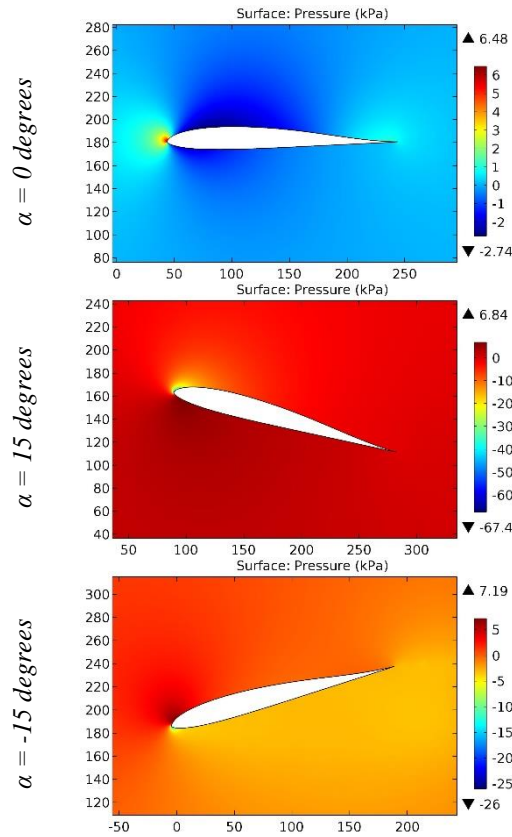


Figure 67. The pressure contours on the surfaces of the MH 45 airfoil.

Impact Factor:

SIS (USA) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

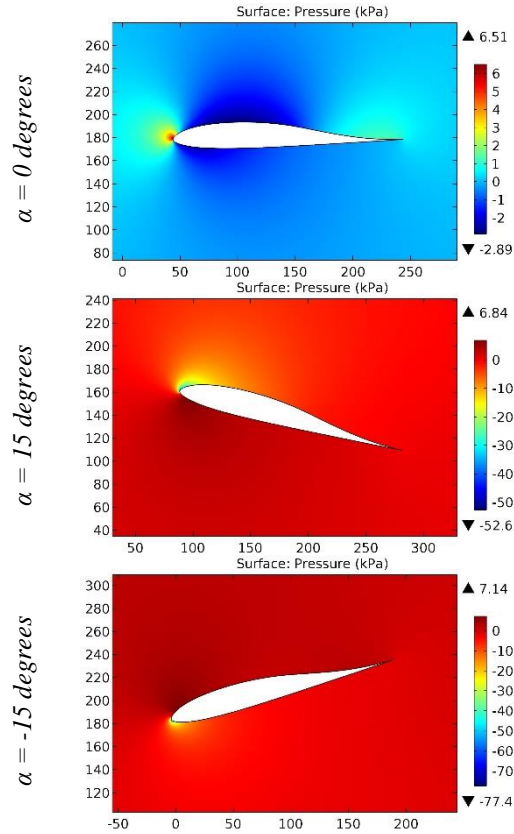


Figure 68. The pressure contours on the surfaces of the MH 46 airfoil.

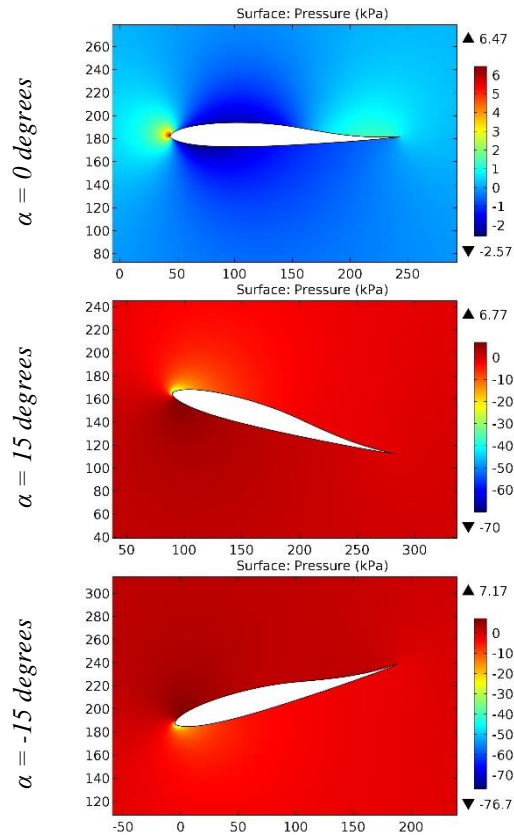


Figure 69. The pressure contours on the surfaces of the MH 49 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

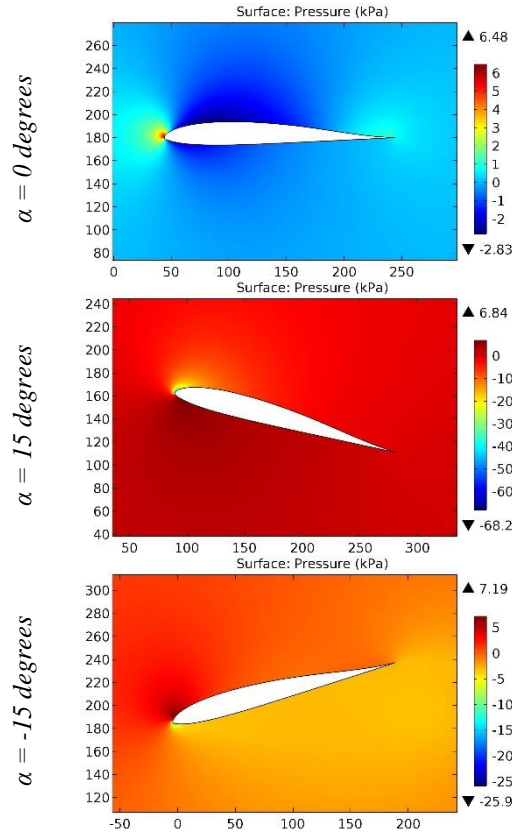


Figure 70. The pressure contours on the surfaces of the MH 60 airfoil.

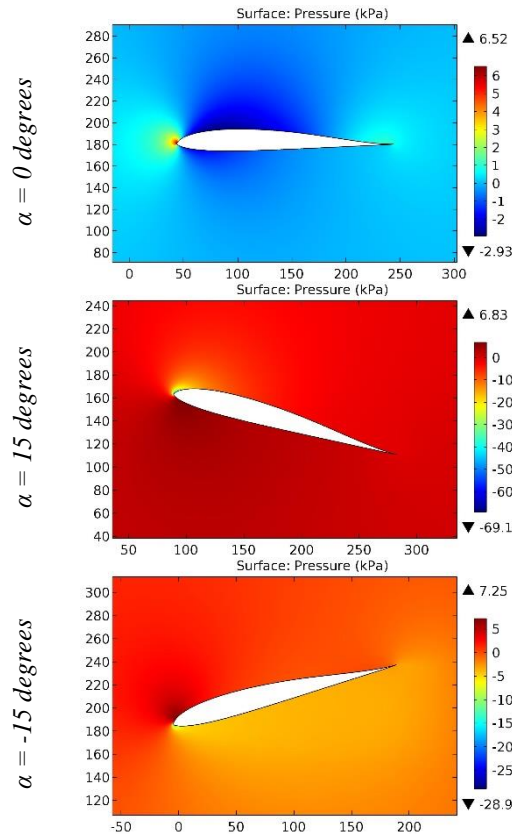


Figure 71. The pressure contours on the surfaces of the MH 60 10,08% airfoil.

Impact Factor:

SIS (USA) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

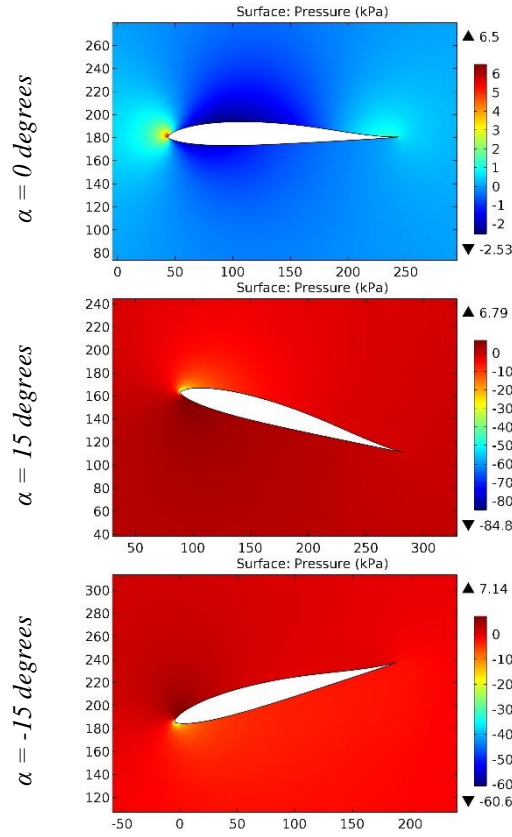


Figure 72. The pressure contours on the surfaces of the MH 61 airfoil.

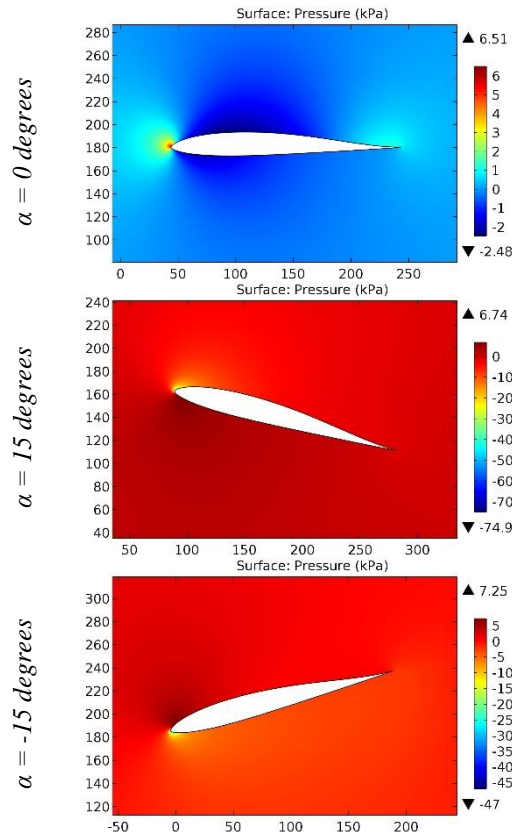


Figure 73. The pressure contours on the surfaces of the MH 61 10,28% airfoil.

Impact Factor:

SISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

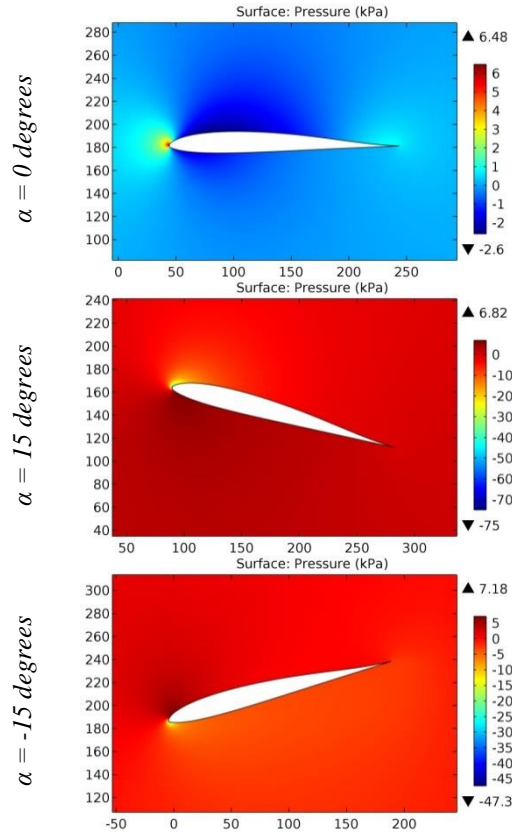


Figure 74. The pressure contours on the surfaces of the MH 62 airfoil.

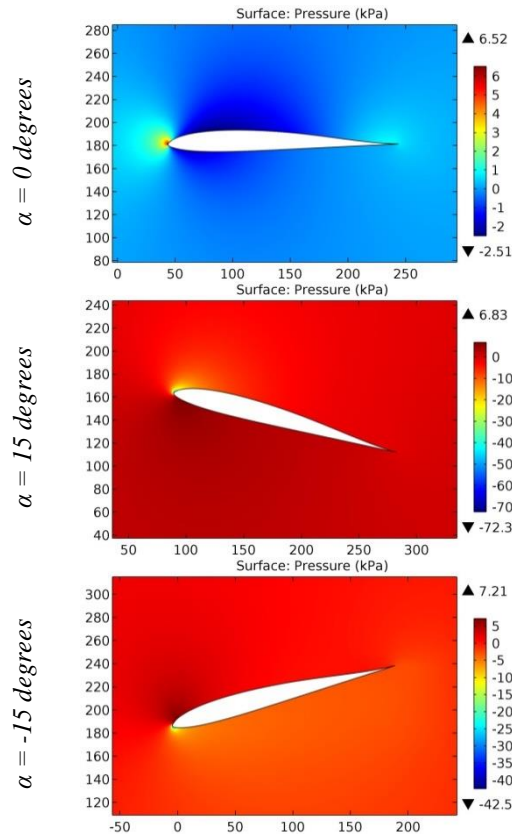


Figure 75. The pressure contours on the surfaces of the MH 62 9,3% airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

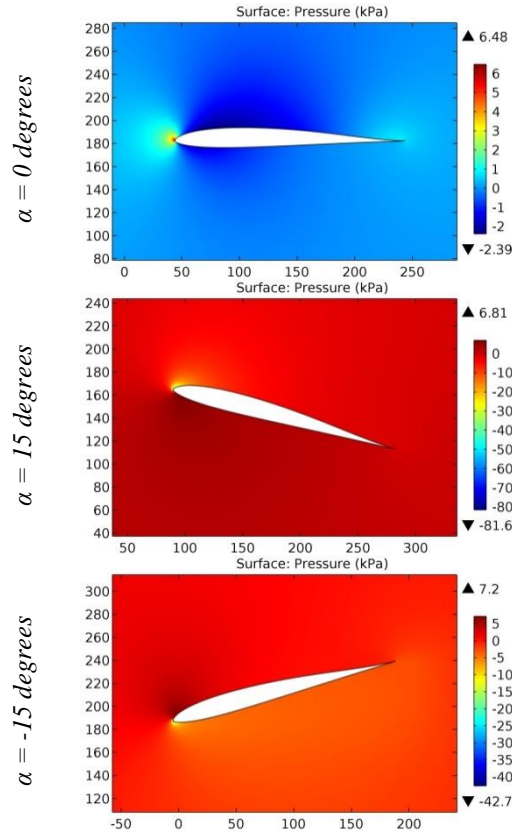


Figure 76. The pressure contours on the surfaces of the MH 64 airfoil.

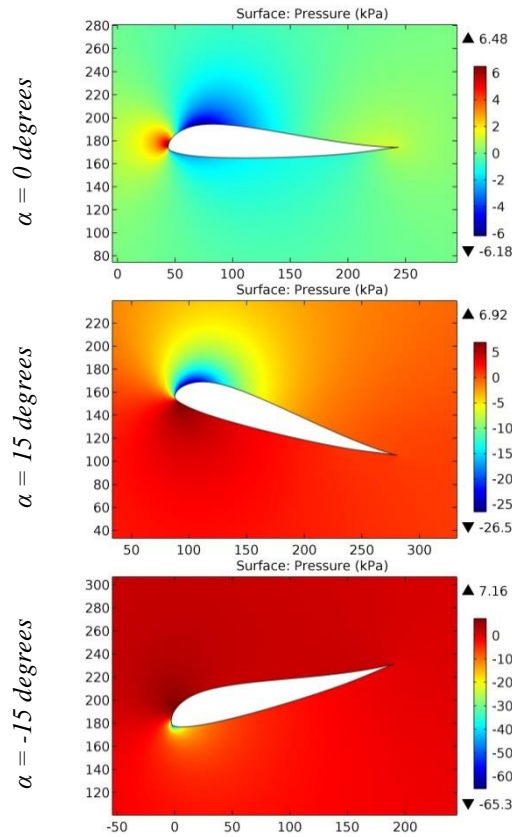


Figure 77. The pressure contours on the surfaces of the MH 78 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

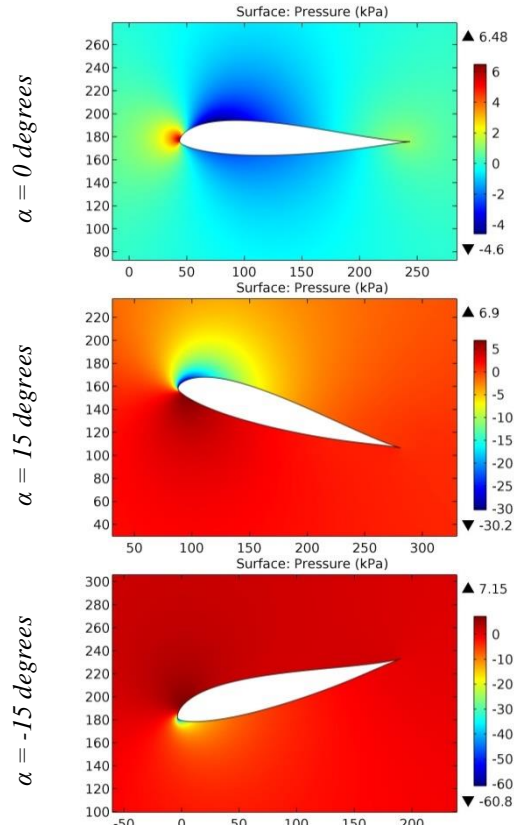


Figure 78. The pressure contours on the surfaces of the MH 91 airfoil.

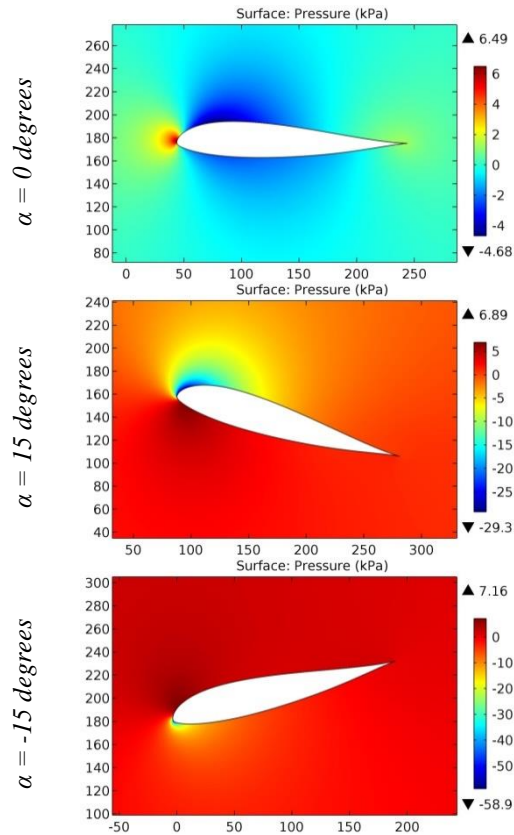


Figure 79. The pressure contours on the surfaces of the MH 92 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

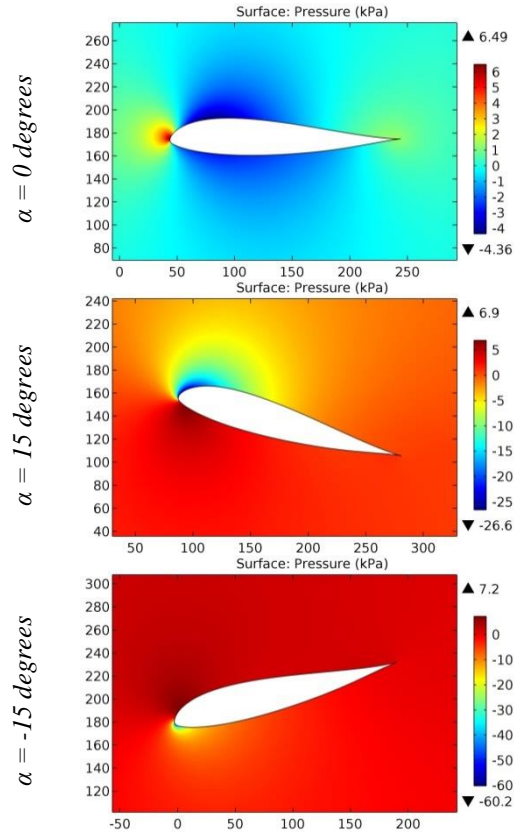


Figure 80. The pressure contours on the surfaces of the MH 93 airfoil.

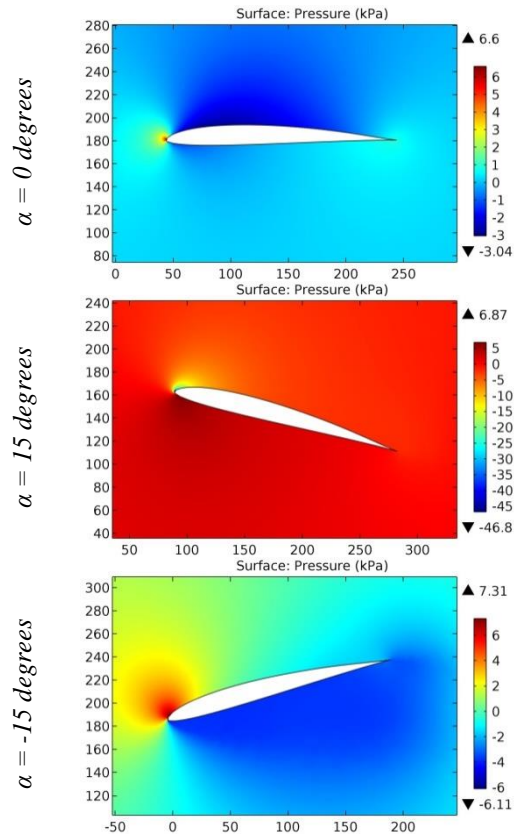


Figure 81. The pressure contours on the surfaces of the MH32 (8,71%) airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

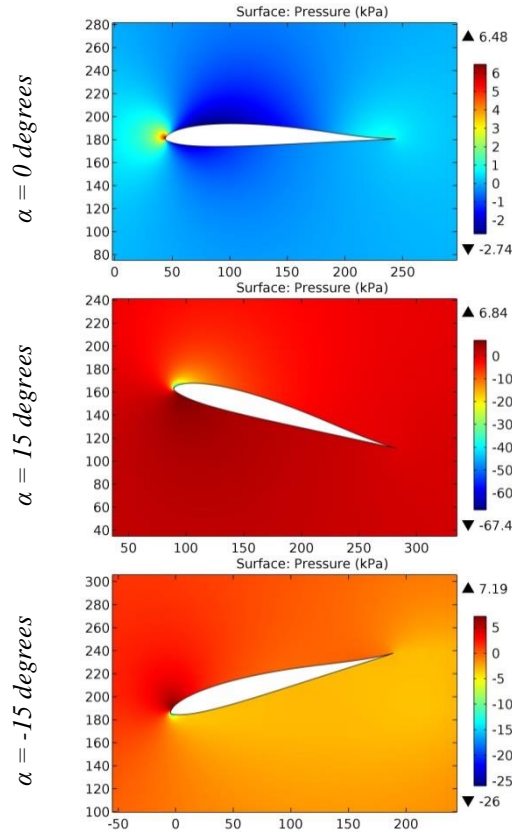


Figure 82. The pressure contours on the surfaces of the MH45 airfoil.

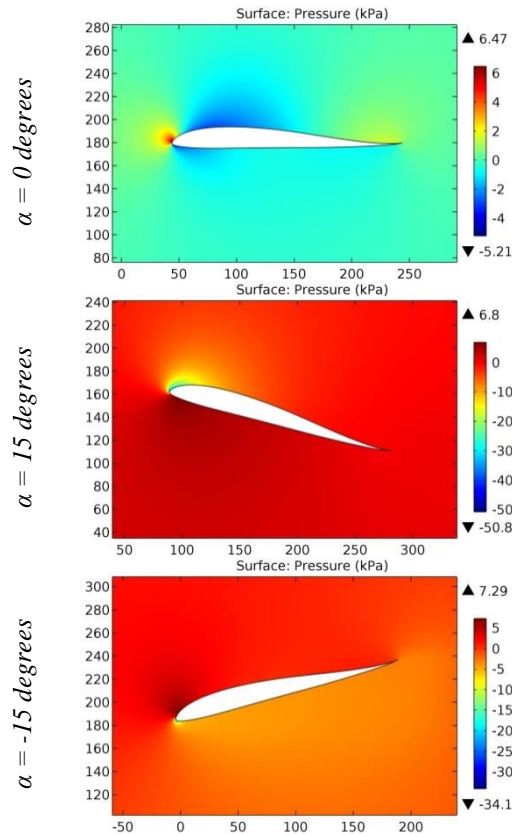


Figure 83. The pressure contours on the surfaces of the mhmi2 airfoil.

Impact Factor:

SIS (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

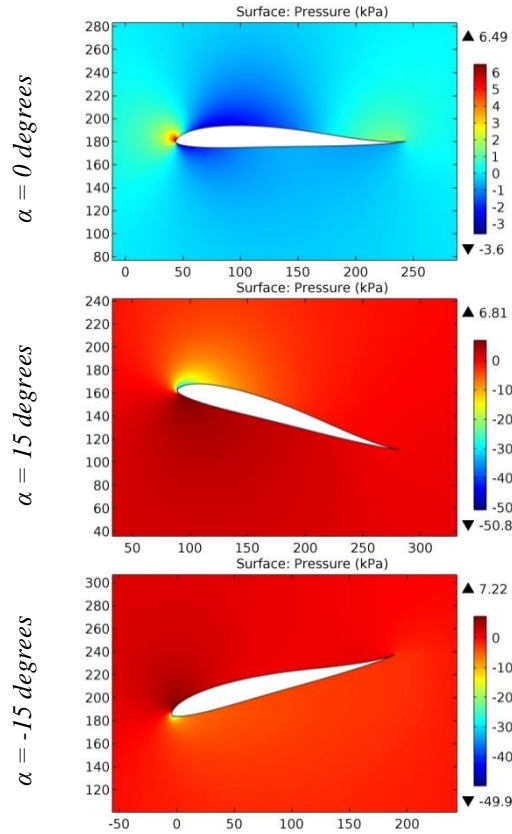


Figure 84. The pressure contours on the surfaces of the mhmi3 airfoil.

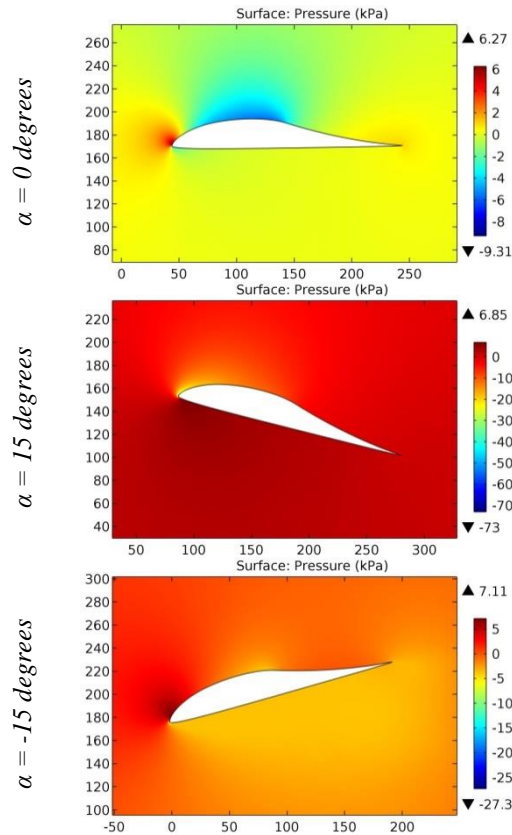


Figure 85. The pressure contours on the surfaces of the MILEY M06-13-128 airfoil.

Impact Factor:

SIS (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

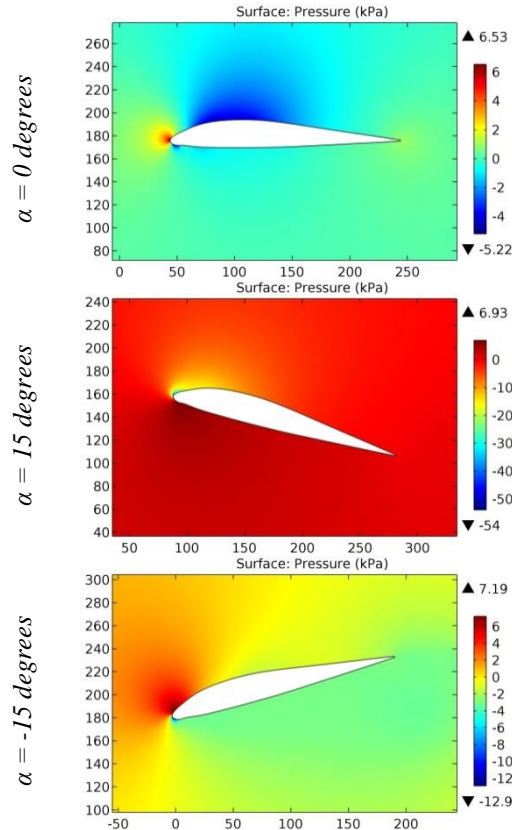


Figure 86. The pressure contours on the surfaces of the MIRAGE airfoil.

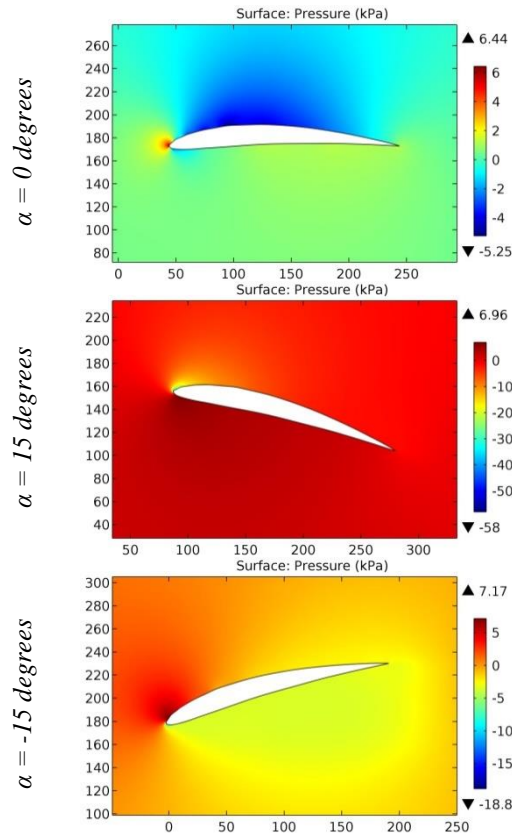


Figure 87. The pressure contours on the surfaces of the Miser airfoil.

Impact Factor:

SISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

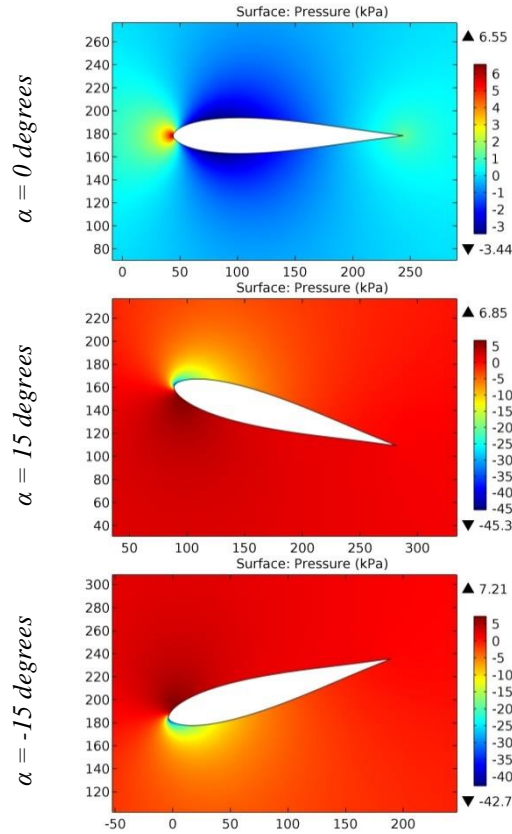


Figure 88. The pressure contours on the surfaces of the Misto 50-50 S1046-S8035 airfoil.

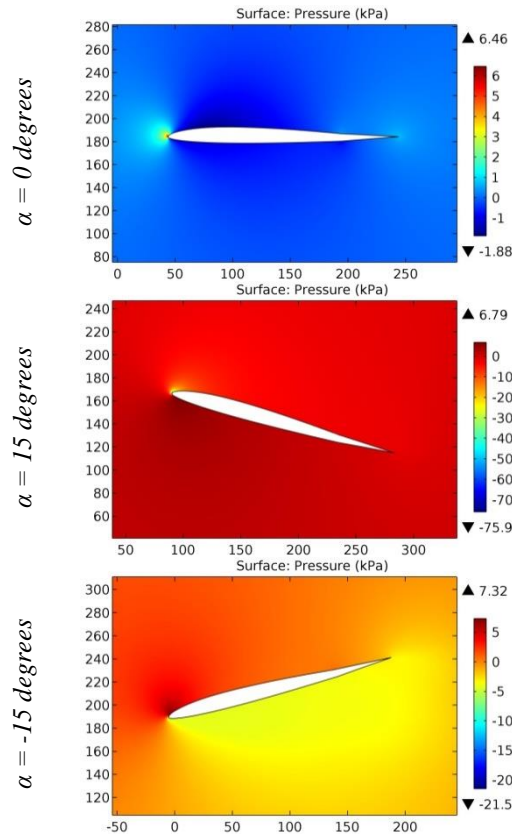


Figure 89. The pressure contours on the surfaces of the mjp711f-3 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

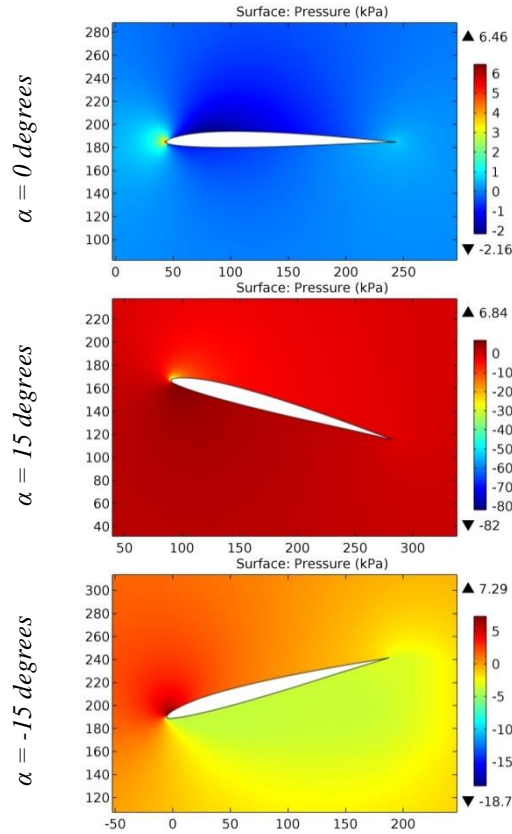


Figure 90. The pressure contours on the surfaces of the mjp712 airfoil.

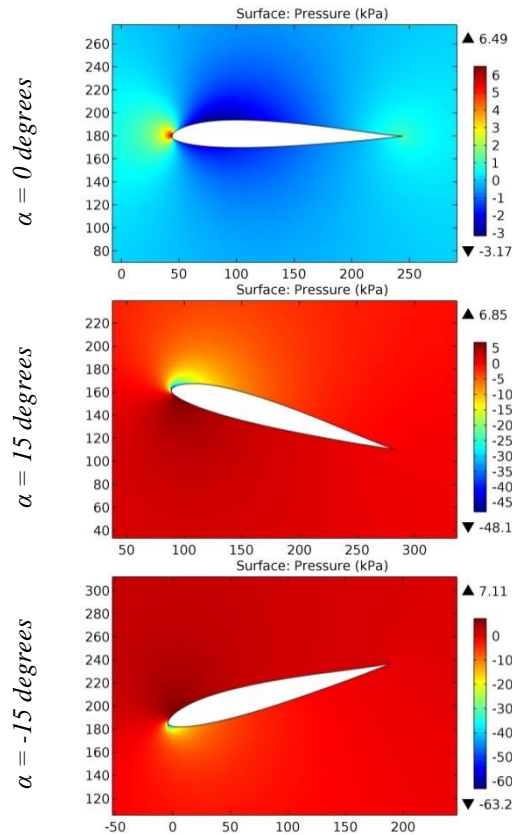


Figure 91. The pressure contours on the surfaces of the mjp1211 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

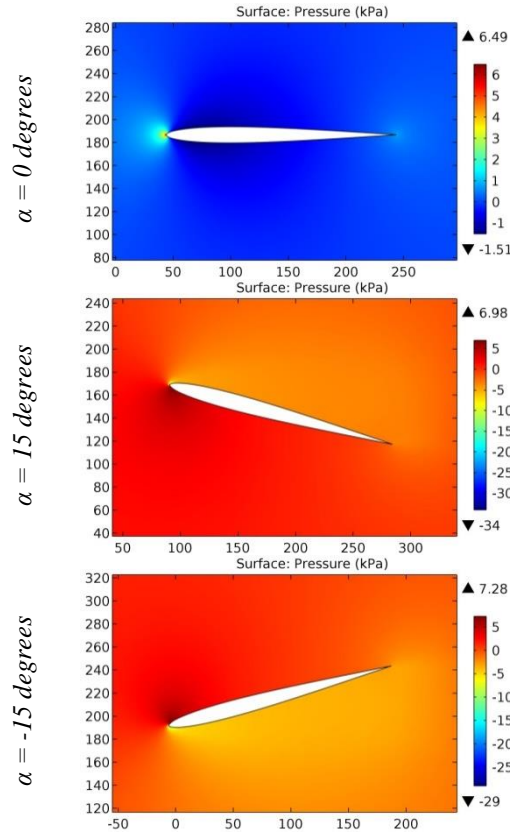


Figure 92. The pressure contours on the surfaces of the MM 007 airfoil.

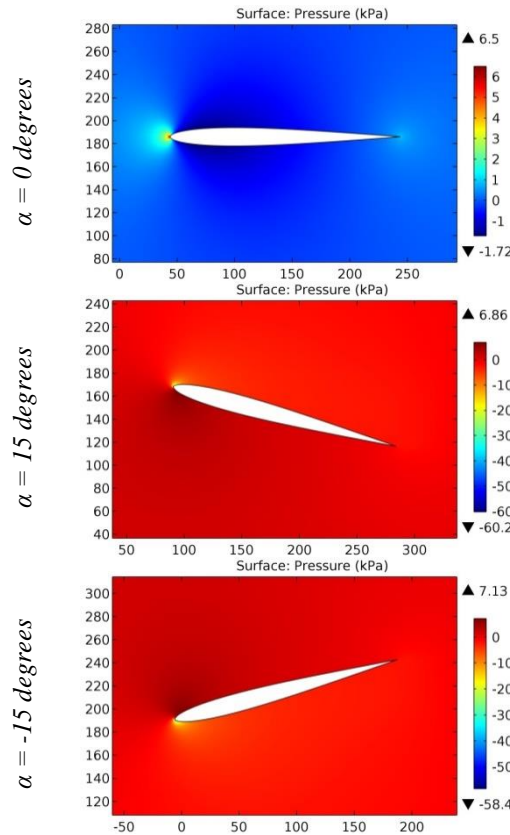


Figure 93. The pressure contours on the surfaces of the MM 008 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

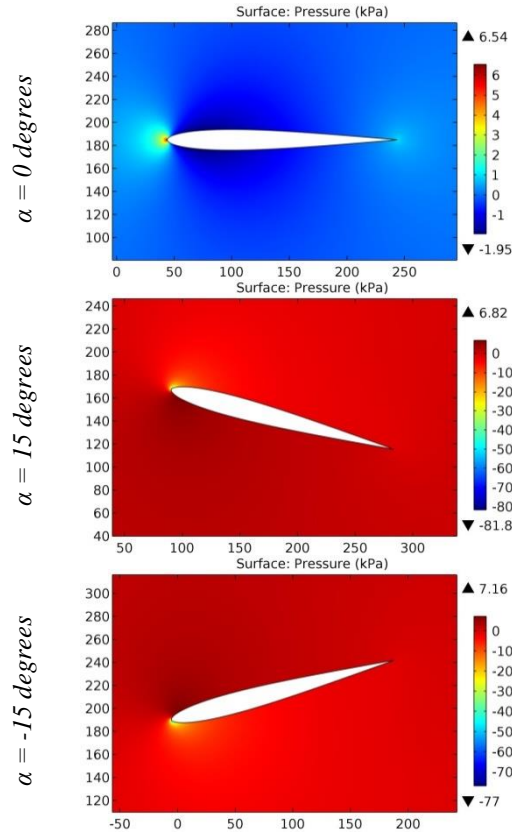


Figure 94. The pressure contours on the surfaces of the MM 009 airfoil.

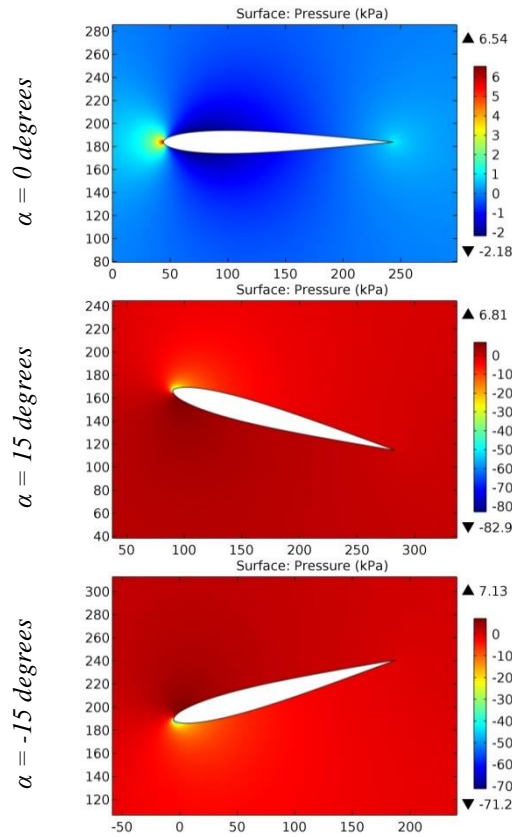


Figure 95. The pressure contours on the surfaces of the MM 010 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

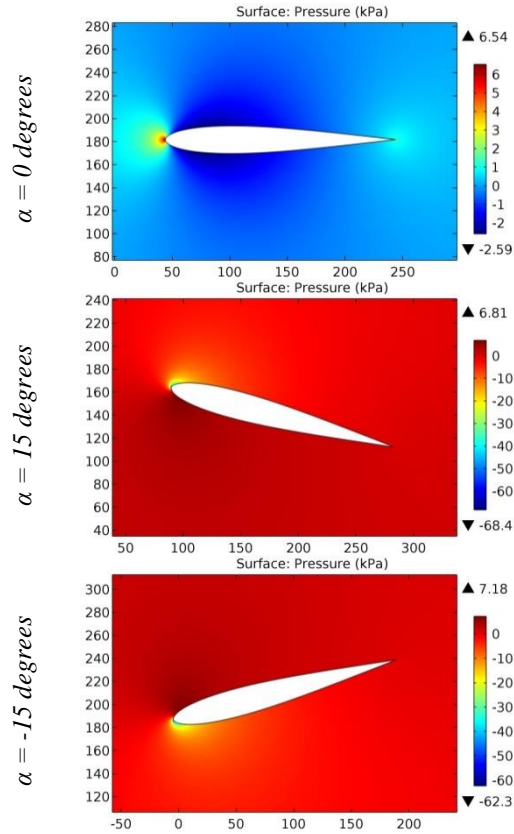


Figure 96. The pressure contours on the surfaces of the MM 012 airfoil.

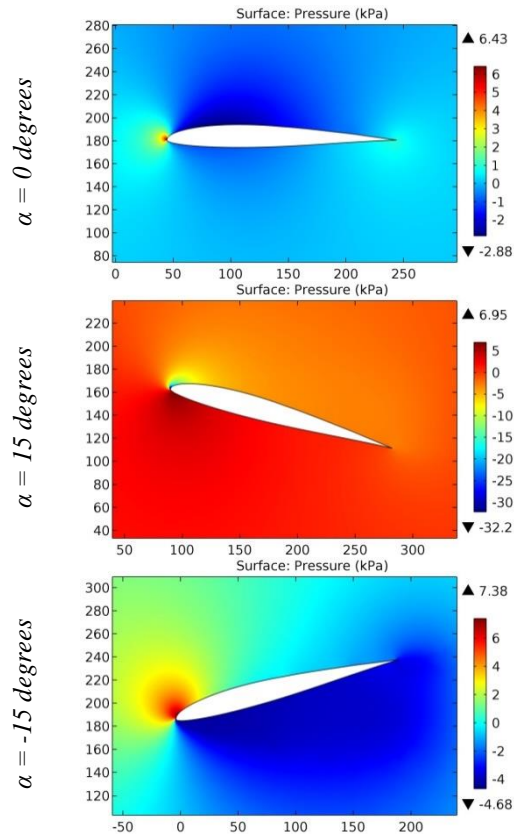


Figure 97. The pressure contours on the surfaces of the MM 1,75-10 airfoil.

Impact Factor:

SISRA (India)	= 6.317	SIS (USA)	= 0.912	ICV (Poland)	= 6.630
ISI (Dubai, UAE)	= 1.582	ПИИЦ (Russia)	= 3.939	PIF (India)	= 1.940
GIF (Australia)	= 0.564	ESJI (KZ)	= 8.771	IBI (India)	= 4.260
JIF	= 1.500	SJIF (Morocco)	= 7.184	OAJI (USA)	= 0.350

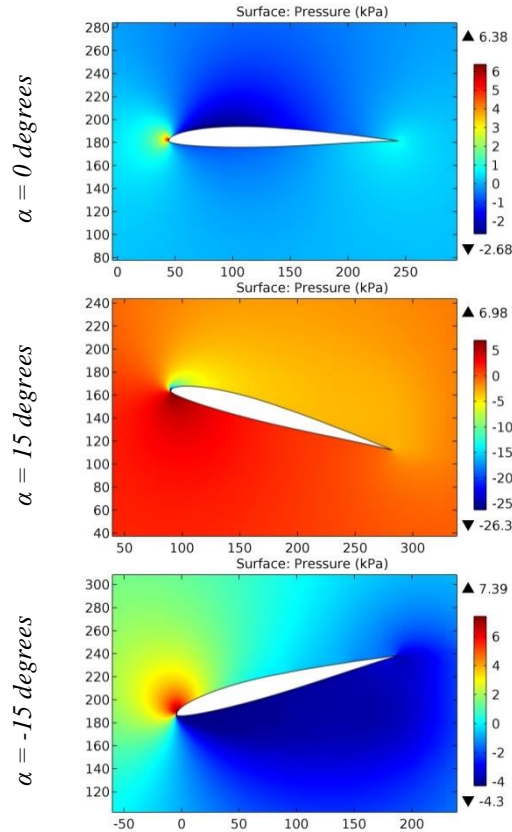


Figure 98. The pressure contours on the surfaces of the MM 1,75-9 airfoil.

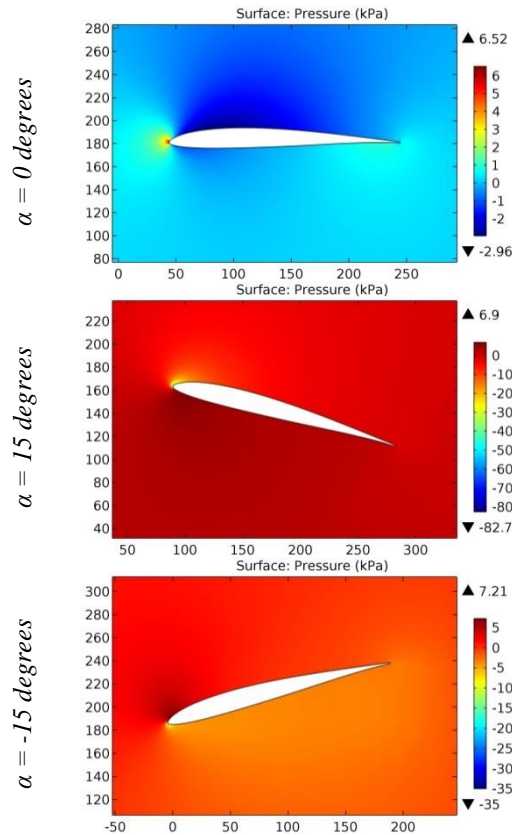


Figure 99. The pressure contours on the surfaces of the MM 100 airfoil.

Impact Factor:

SISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

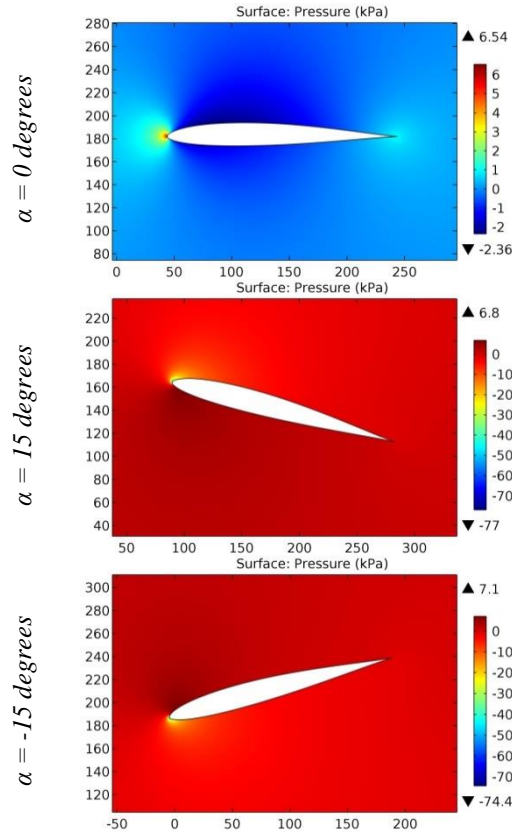


Figure 100. The pressure contours on the surfaces of the MM 1010a airfoil.

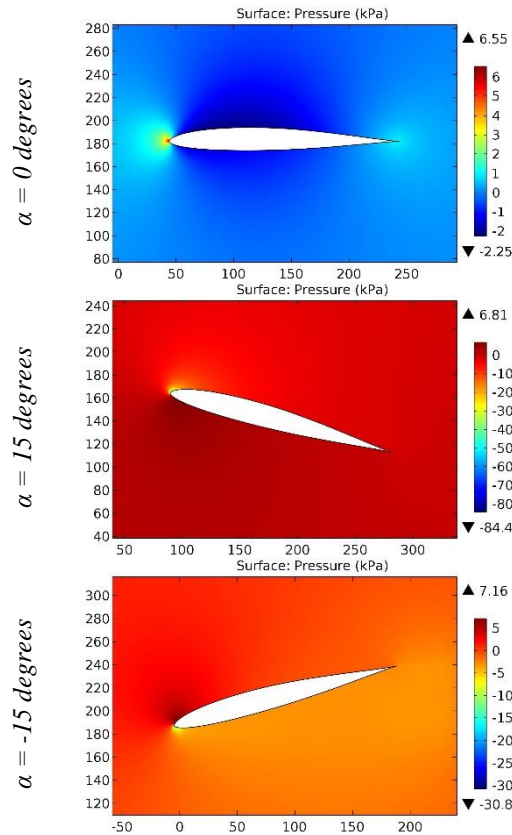


Figure 101. The pressure contours on the surfaces of the MM 1010b airfoil.

Impact Factor:

SISRA (India)	= 6.317	SIS (USA)	= 0.912	ICV (Poland)	= 6.630
ISI (Dubai, UAE)	= 1.582	ПИИЦ (Russia)	= 3.939	PIF (India)	= 1.940
GIF (Australia)	= 0.564	ESJI (KZ)	= 8.771	IBI (India)	= 4.260
JIF	= 1.500	SJIF (Morocco)	= 7.184	OAJI (USA)	= 0.350

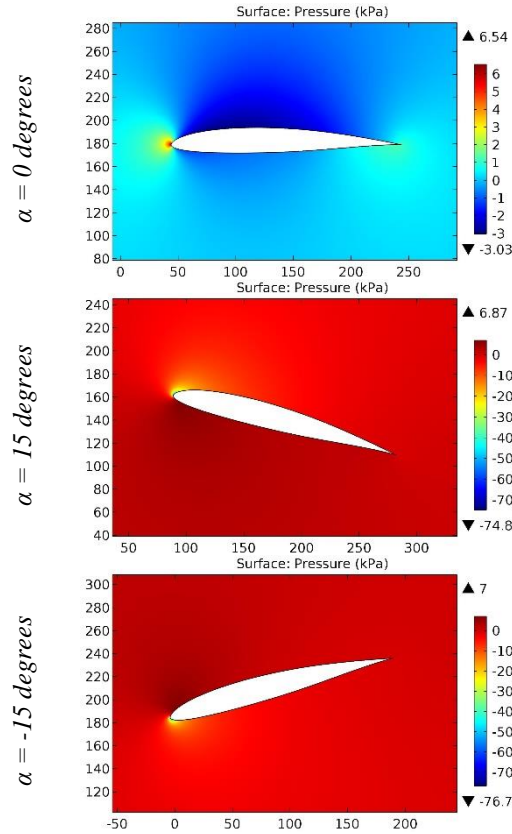


Figure 102. The pressure contours on the surfaces of the MM 1100 airfoil.

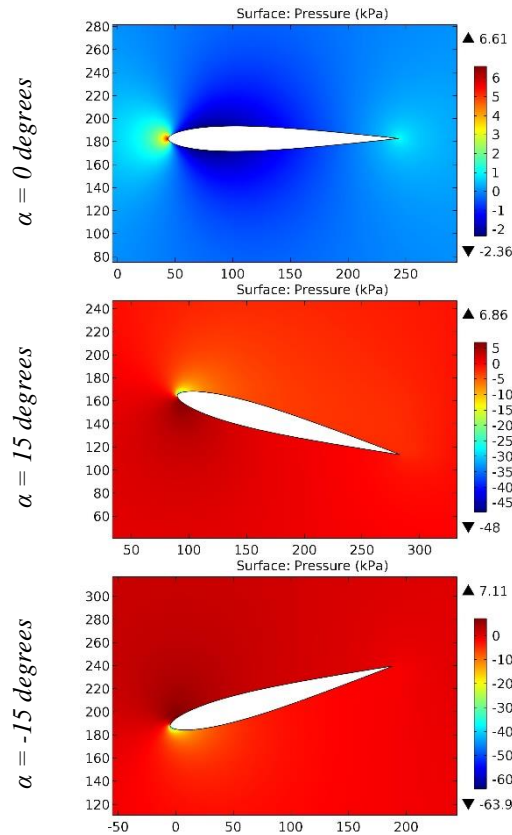


Figure 103. The pressure contours on the surfaces of the MM 11-29 airfoil.

Impact Factor:

SIS (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

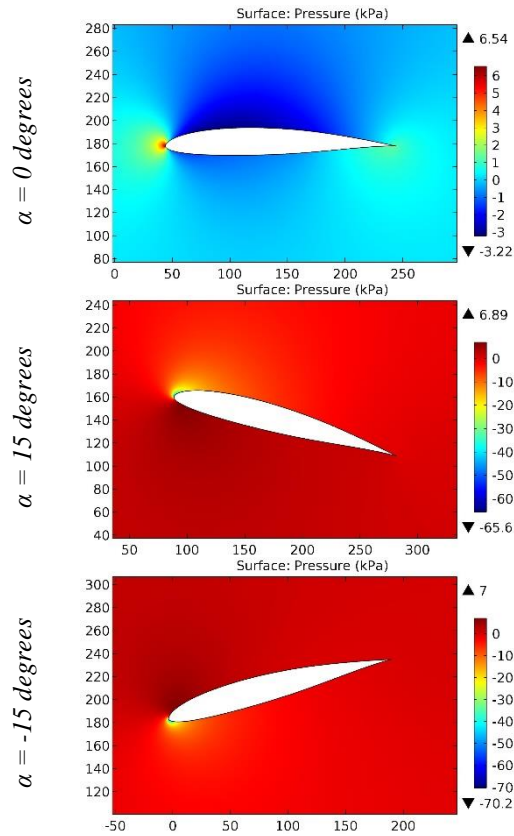


Figure 104. The pressure contours on the surfaces of the MM 1200 airfoil.

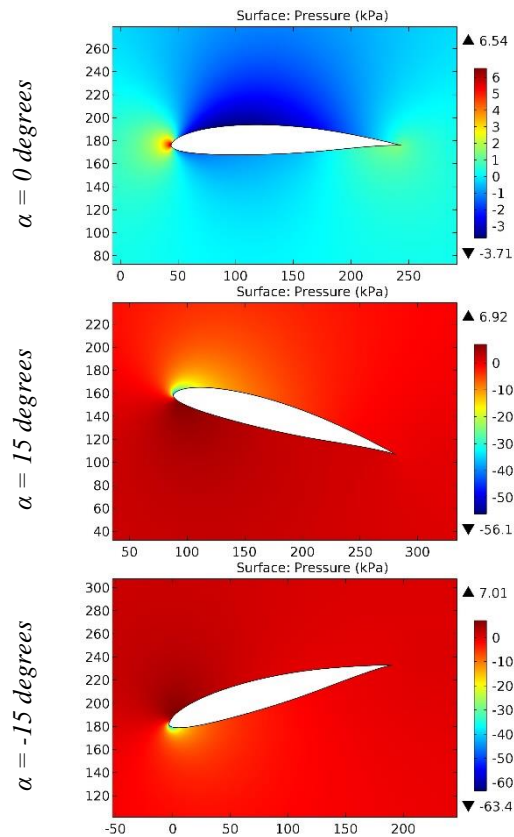


Figure 105. The pressure contours on the surfaces of the MM 1300 airfoil.

Impact Factor:

SIS (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

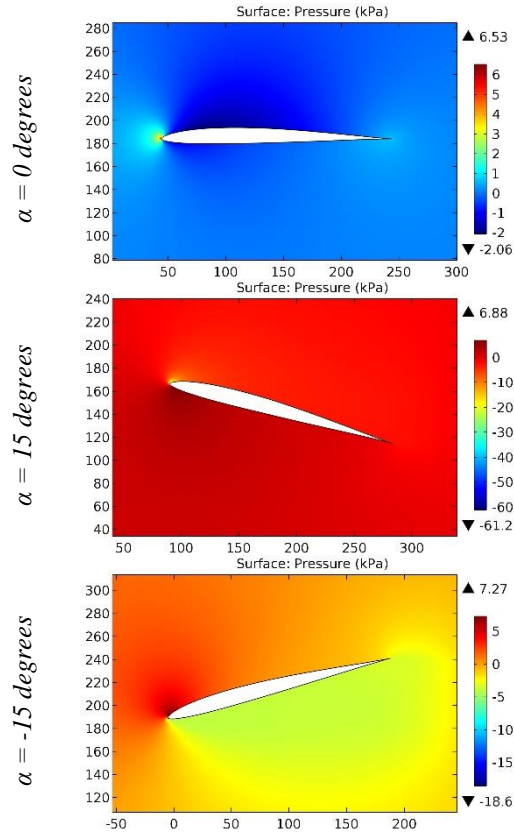


Figure 106. The pressure contours on the surfaces of the MM 1407 airfoil.

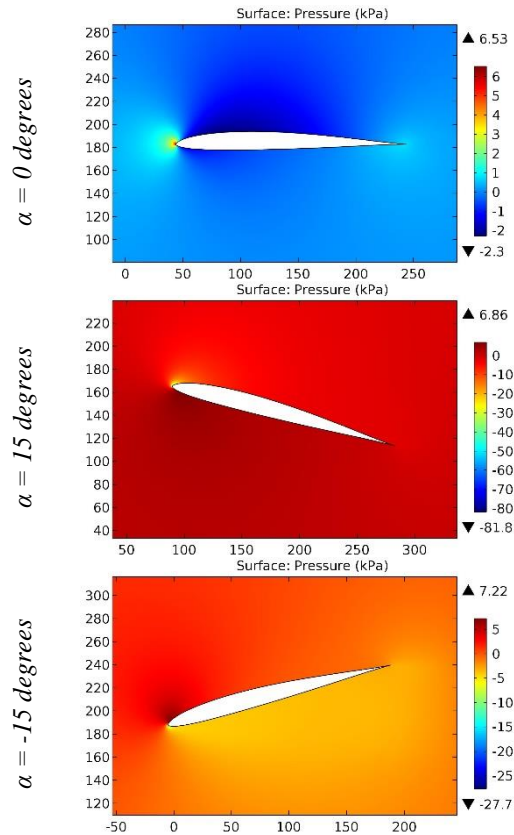


Figure 107. The pressure contours on the surfaces of the MM 1608 airfoil.

Impact Factor:

SISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

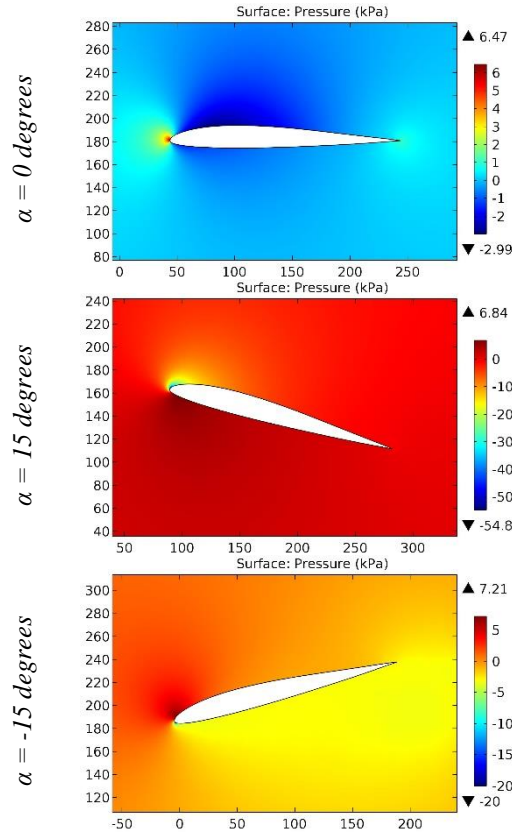


Figure 108. The pressure contours on the surfaces of the MM 1609 airfoil.

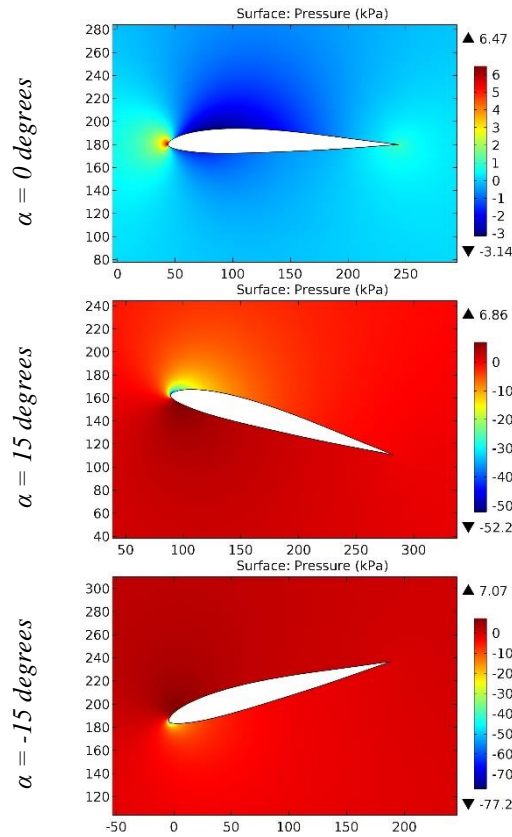


Figure 109. The pressure contours on the surfaces of the MM 1710 airfoil.

Impact Factor:

SIS (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

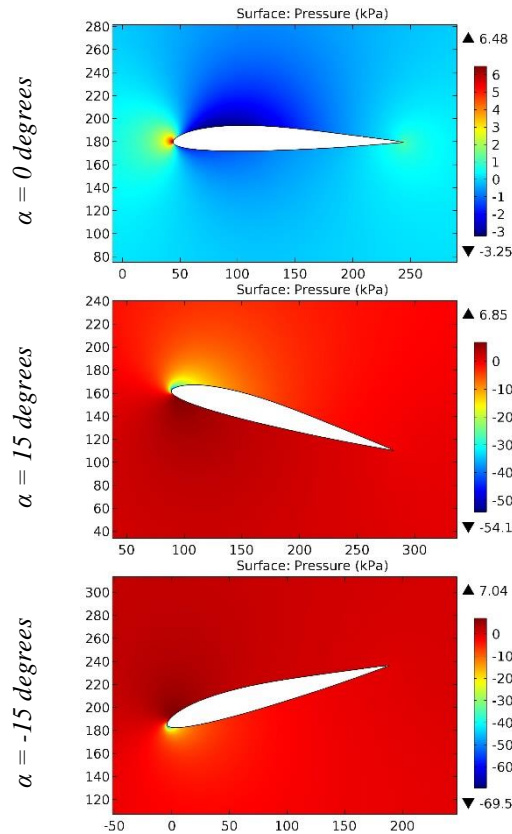


Figure 110. The pressure contours on the surfaces of the MM 1711 airfoil.

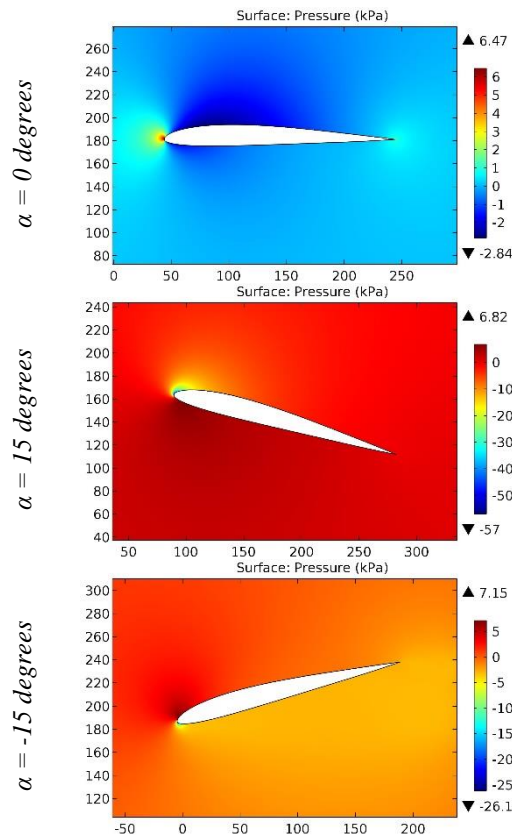


Figure 111. The pressure contours on the surfaces of the MM 1809 airfoil.

Impact Factor:

SISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

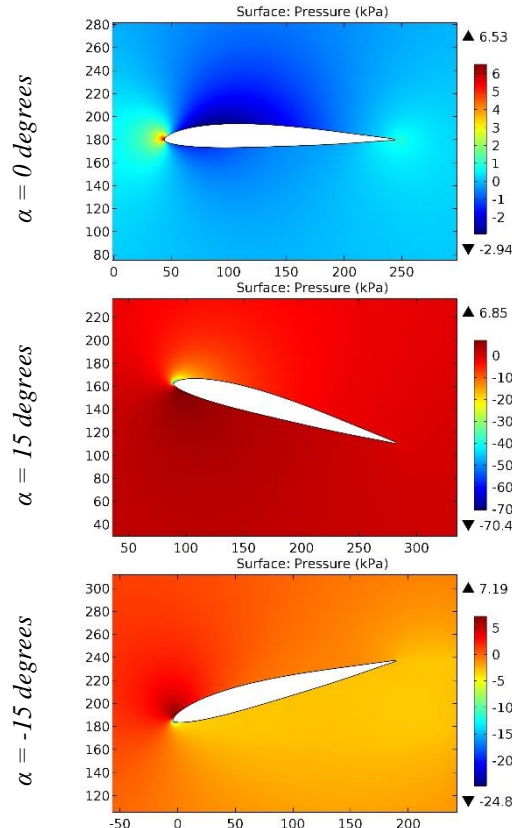


Figure 112. The pressure contours on the surfaces of the MM 1810 airfoil.

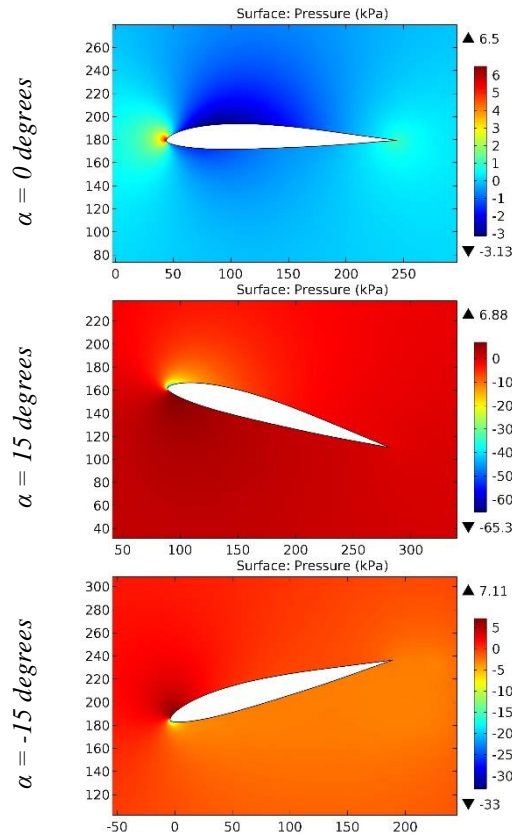


Figure 113. The pressure contours on the surfaces of the MM 1811b airfoil.

Impact Factor:

SIS (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

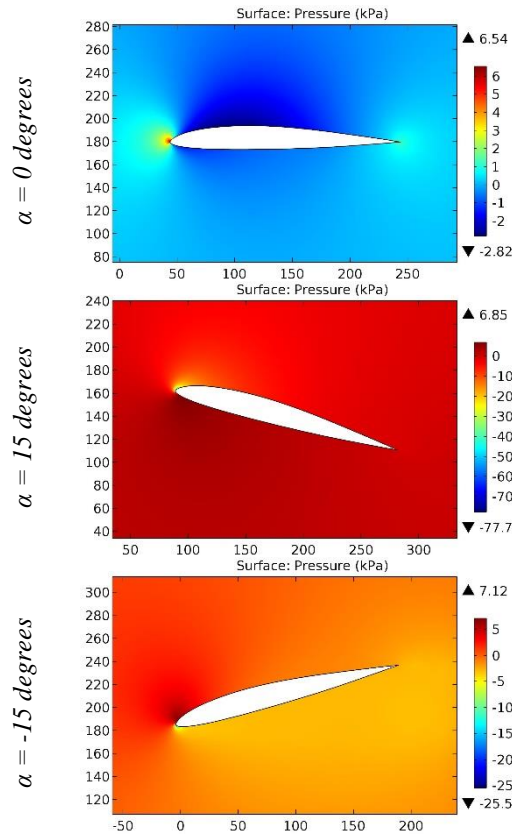


Figure 114. The pressure contours on the surfaces of the MM 1910 airfoil.

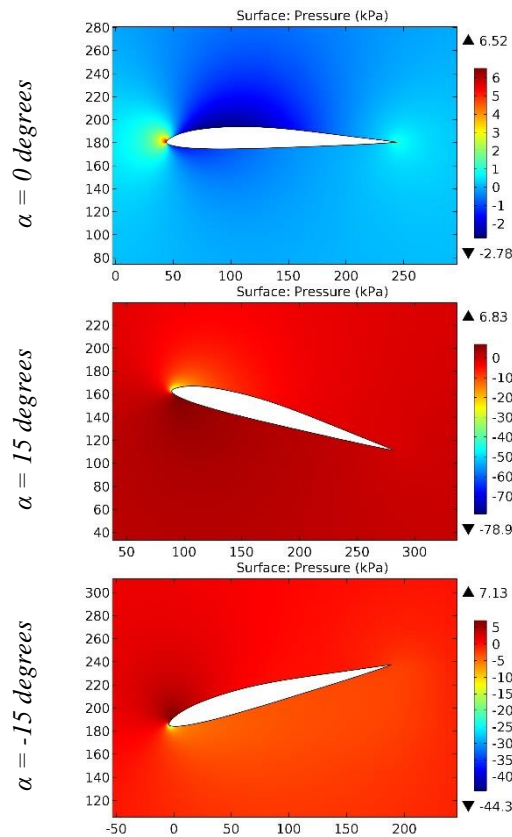


Figure 115. The pressure contours on the surfaces of the MM 1995 airfoil.

Impact Factor:

SISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

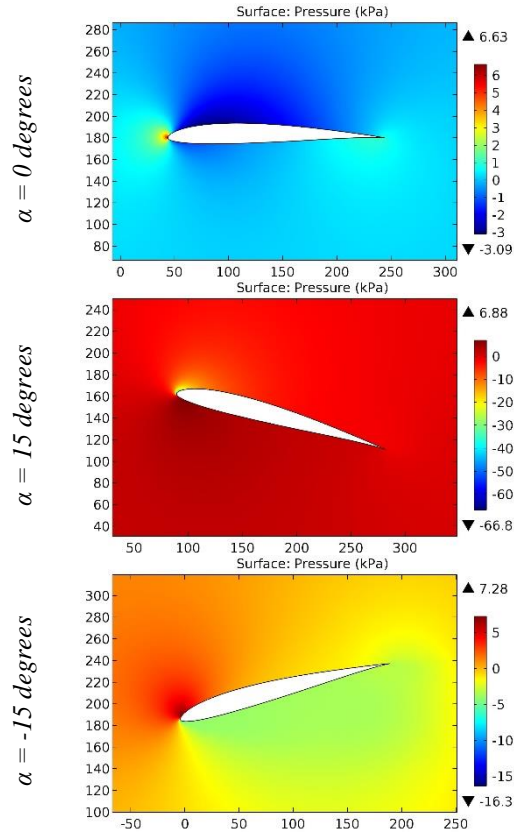


Figure 116. The pressure contours on the surfaces of the MM 200 airfoil.

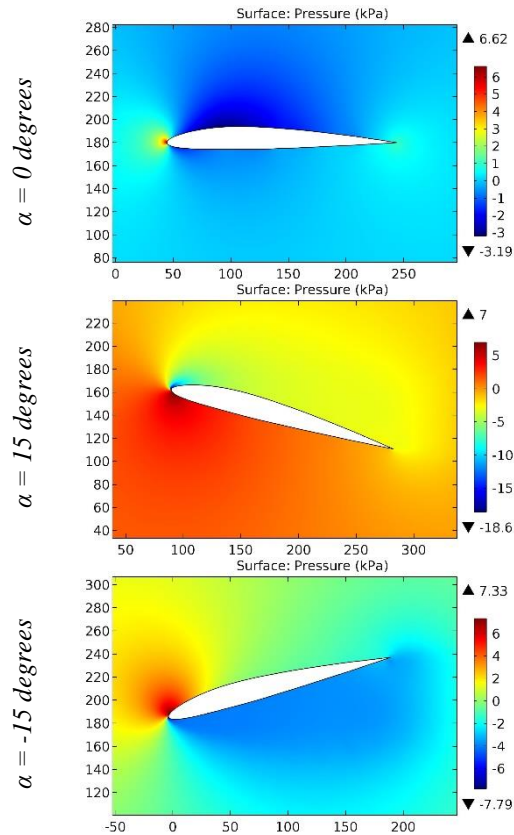


Figure 117. The pressure contours on the surfaces of the MM 2-10 a airfoil.

Impact Factor:

SISRA (India)	= 6.317	SIS (USA)	= 0.912	ICV (Poland)	= 6.630
ISI (Dubai, UAE)	= 1.582	ПИИЦ (Russia)	= 3.939	PIF (India)	= 1.940
GIF (Australia)	= 0.564	ESJI (KZ)	= 8.771	IBI (India)	= 4.260
JIF	= 1.500	SJIF (Morocco)	= 7.184	OAJI (USA)	= 0.350

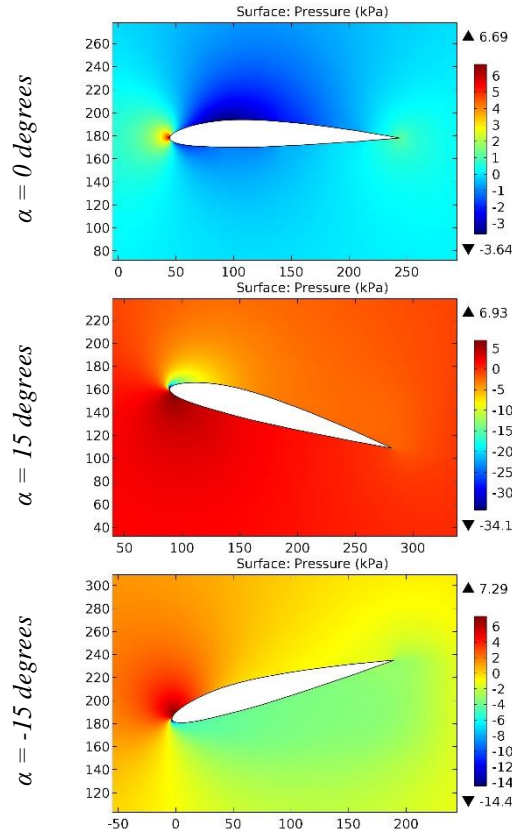


Figure 118. The pressure contours on the surfaces of the MM 2-12 airfoil.

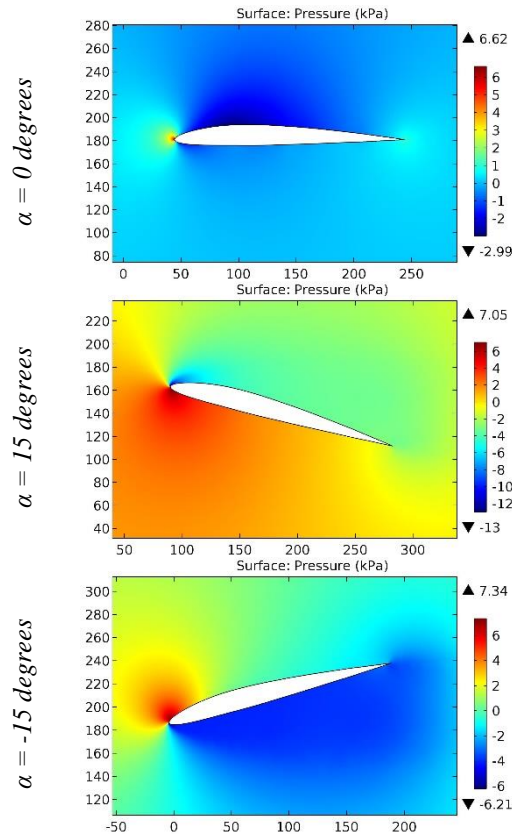


Figure 119. The pressure contours on the surfaces of the MM 2-9 airfoil.

Impact Factor:

SISRA (India)	= 6.317	SIS (USA)	= 0.912	ICV (Poland)	= 6.630
ISI (Dubai, UAE)	= 1.582	ПИИЦ (Russia)	= 3.939	PIF (India)	= 1.940
GIF (Australia)	= 0.564	ESJI (KZ)	= 8.771	IBI (India)	= 4.260
JIF	= 1.500	SJIF (Morocco)	= 7.184	OAJI (USA)	= 0.350

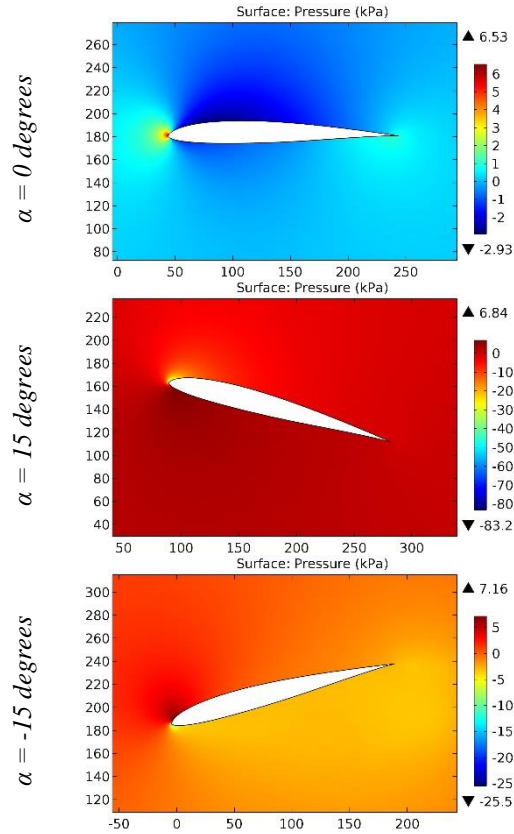


Figure 120. The pressure contours on the surfaces of the MM 300 airfoil.

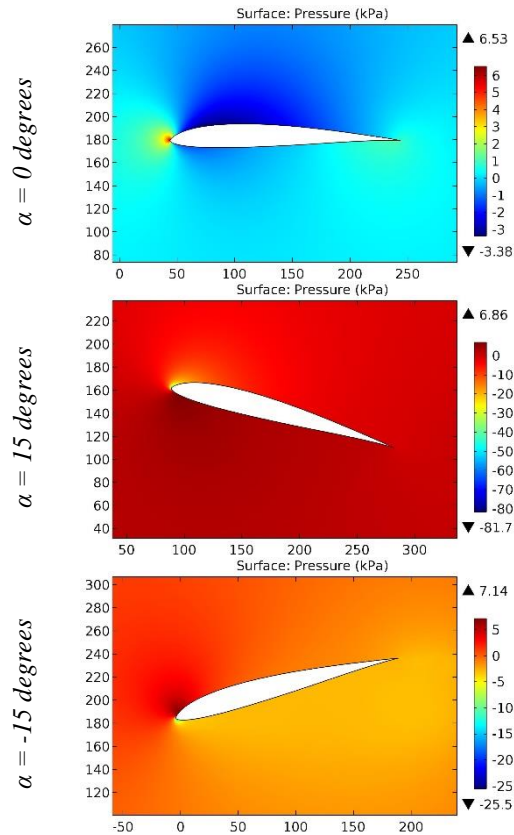


Figure 121. The pressure contours on the surfaces of the MM 400 airfoil.

Impact Factor:

SIS (USA)	= 6.317	SIS (USA)	= 0.912	ICV (Poland)	= 6.630
ISI (Dubai, UAE)	= 1.582	ПИИЦ (Russia)	= 3.939	PIF (India)	= 1.940
GIF (Australia)	= 0.564	ESJI (KZ)	= 8.771	IBI (India)	= 4.260
JIF	= 1.500	SJIF (Morocco)	= 7.184	OAJI (USA)	= 0.350

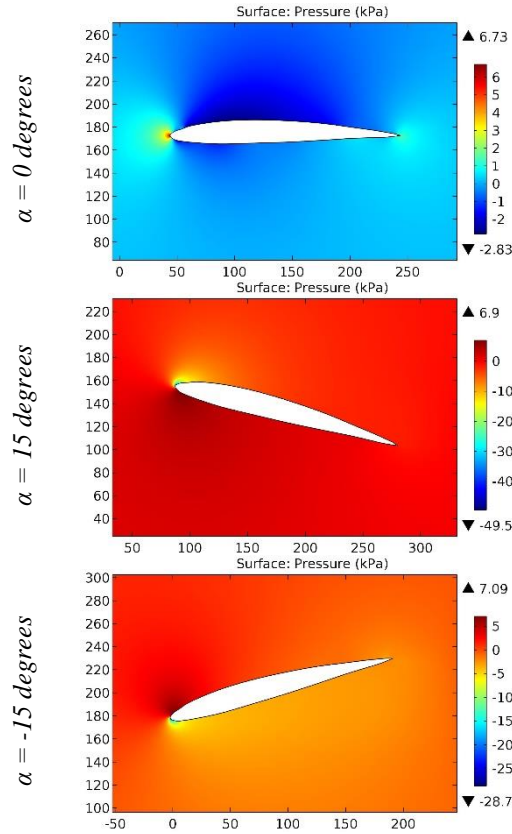


Figure 122. The pressure contours on the surfaces of the Mosca 317 airfoil.

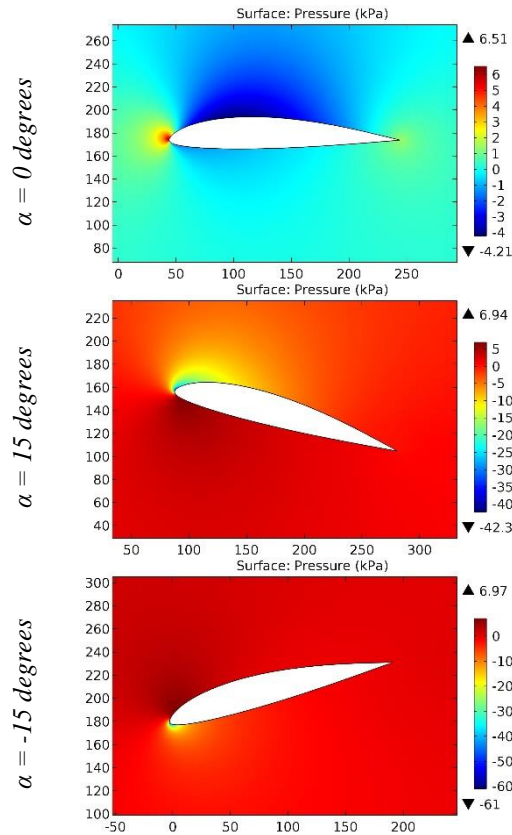


Figure 123. The pressure contours on the surfaces of the MRC-16 airfoil.

Impact Factor:

SISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

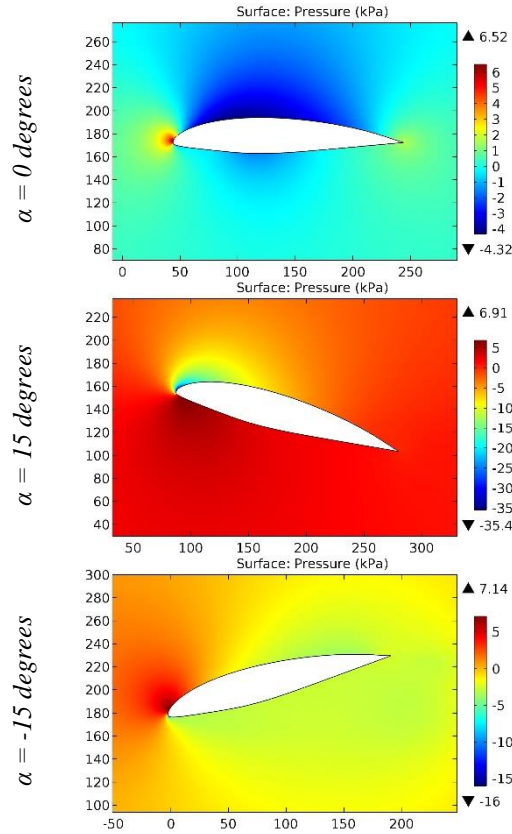


Figure 124. The pressure contours on the surfaces of the MRC-20 airfoil.

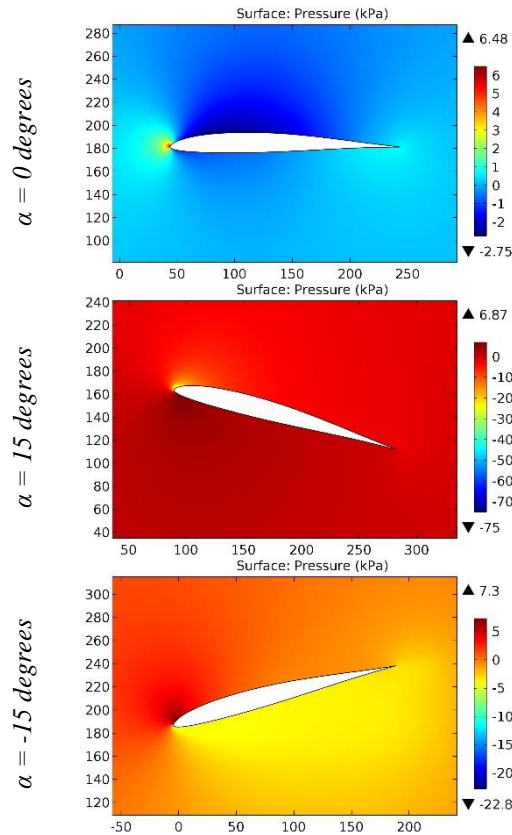


Figure 125. The pressure contours on the surfaces of the ms1,9-8,7 airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

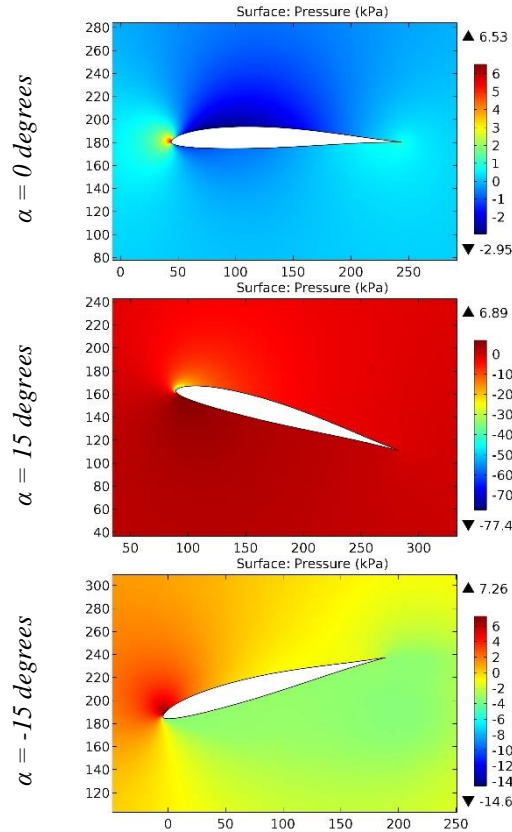


Figure 126. The pressure contours on the surfaces of the ms2-9,5 airfoil.

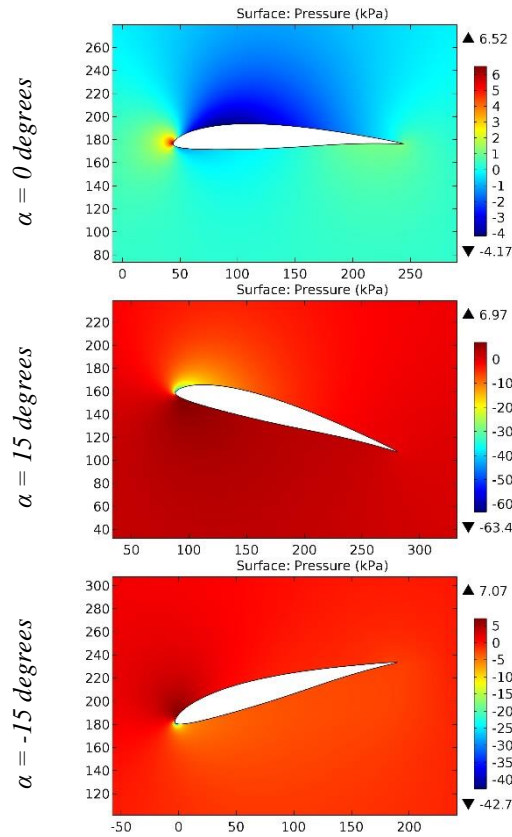


Figure 127. The pressure contours on the surfaces of the MS3,3-11GP airfoil.

Impact Factor:

ISRA (India) = 6.317	SIS (USA) = 0.912	ICV (Poland) = 6.630
ISI (Dubai, UAE) = 1.582	ПИИЦ (Russia) = 3.939	PIF (India) = 1.940
GIF (Australia) = 0.564	ESJI (KZ) = 8.771	IBI (India) = 4.260
JIF = 1.500	SJIF (Morocco) = 7.184	OAJI (USA) = 0.350

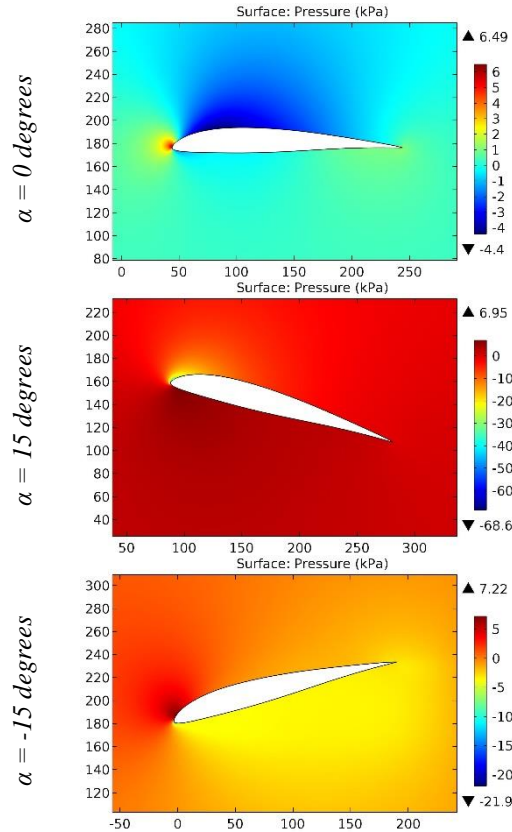


Figure 128. The pressure contours on the surfaces of the MS3,3-11GPT airfoil.

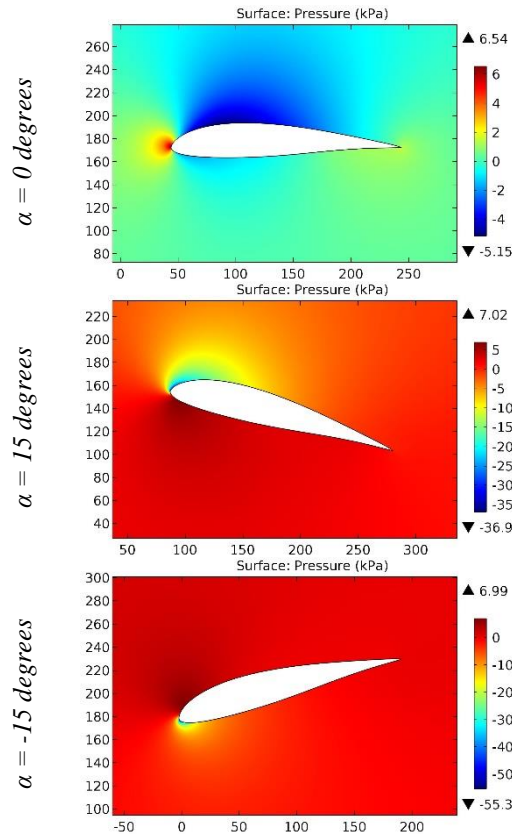


Figure 129. The pressure contours on the surfaces of the MS3,3-15GP airfoil.

Impact Factor:

SISRA (India)	= 6.317	SIS (USA)	= 0.912	ICV (Poland)	= 6.630
ISI (Dubai, UAE)	= 1.582	ПИИЦ (Russia)	= 3.939	PIF (India)	= 1.940
GIF (Australia)	= 0.564	ESJI (KZ)	= 8.771	IBI (India)	= 4.260
JIF	= 1.500	SJIF (Morocco)	= 7.184	OAJI (USA)	= 0.350

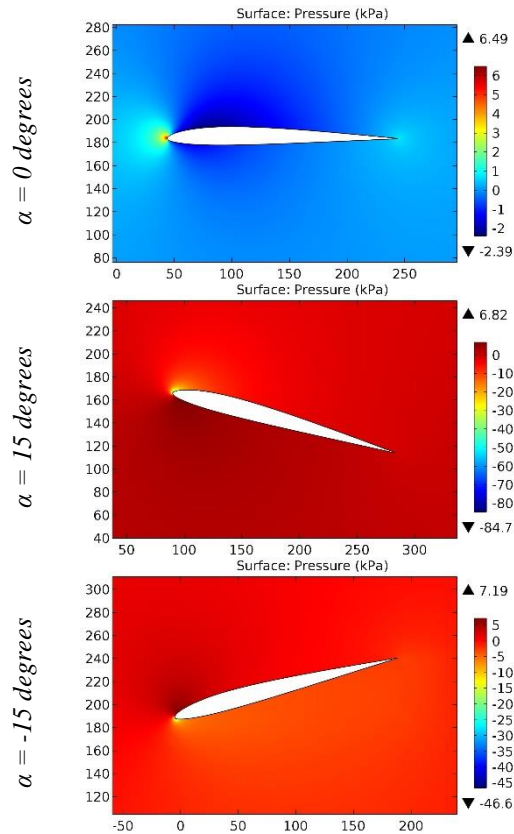


Figure 130. The pressure contours on the surfaces of the msa812 airfoil.

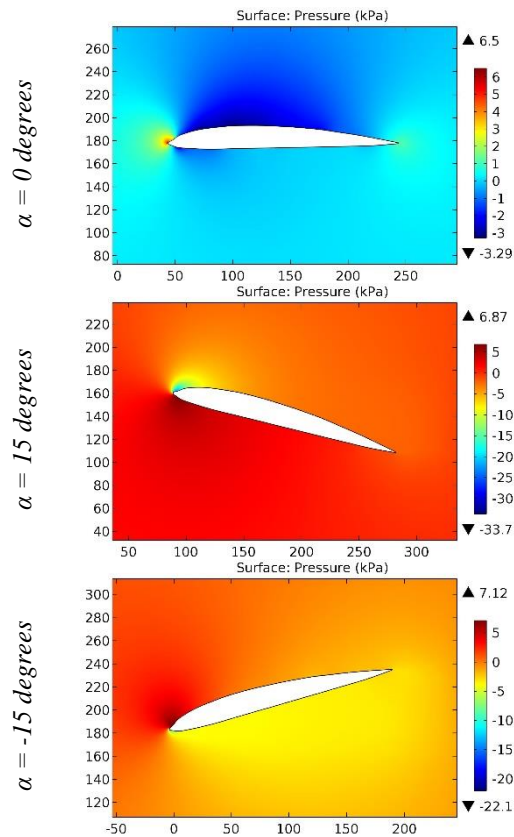


Figure 131. The pressure contours on the surfaces of the MT172 airfoil.

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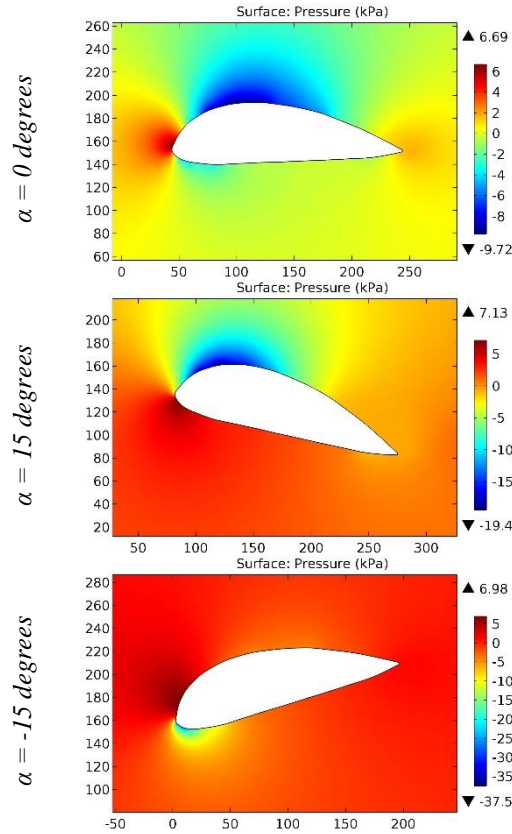


Figure 132. The pressure contours on the surfaces of the MT722 airfoil.

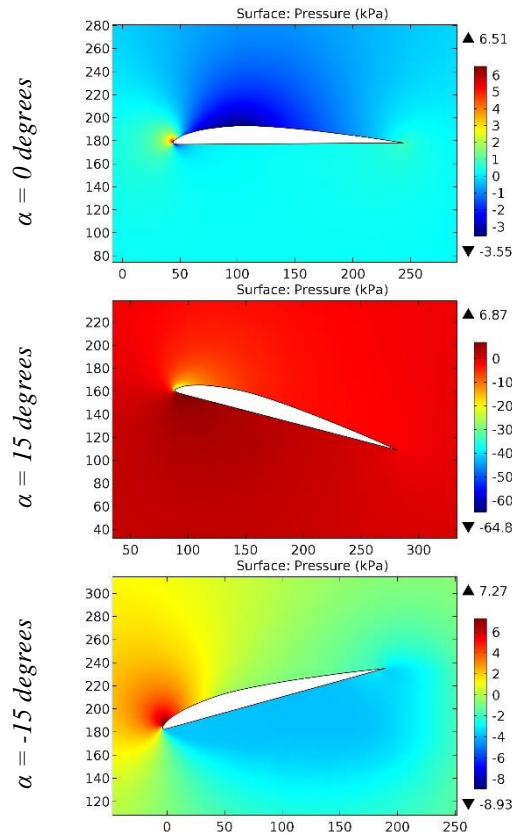


Figure 133. The pressure contours on the surfaces of the MVA-101M airfoil.

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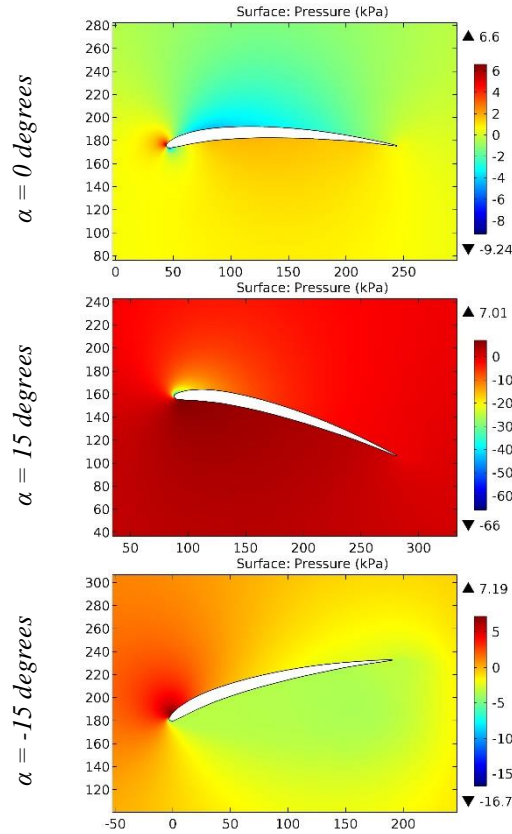


Figure 134. The pressure contours on the surfaces of the MVA-123 airfoil.

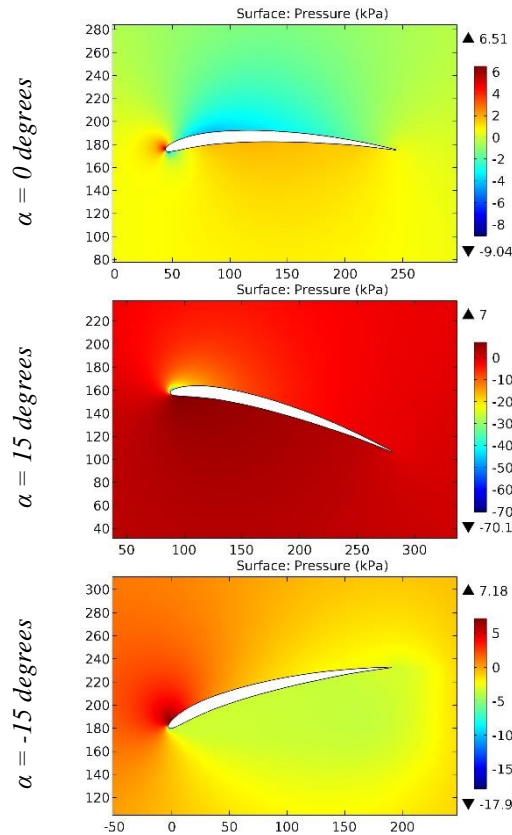


Figure 135. The pressure contours on the surfaces of the MVA-123M airfoil.

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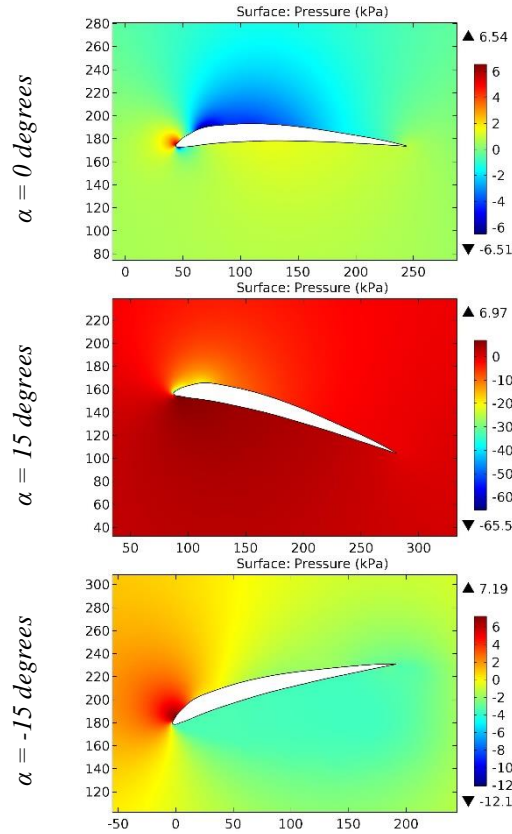


Figure 136. The pressure contours on the surfaces of the MVA-173 airfoil.

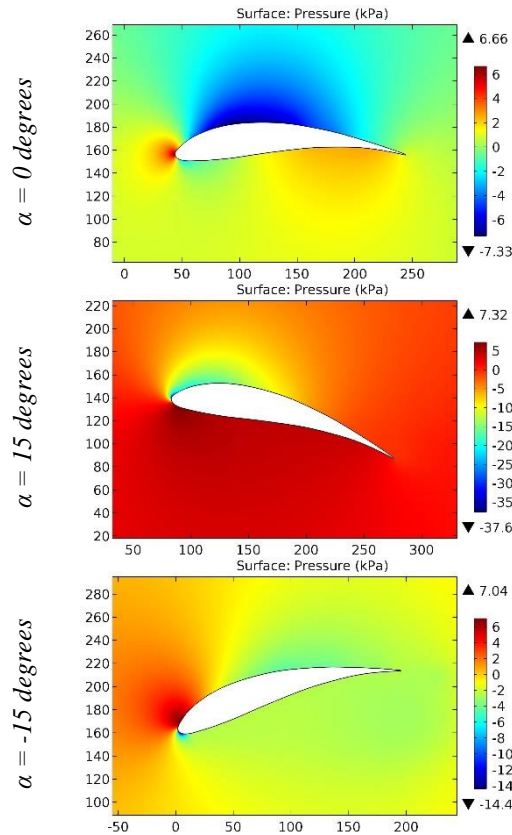


Figure 137. The pressure contours on the surfaces of the MVA-227 airfoil.

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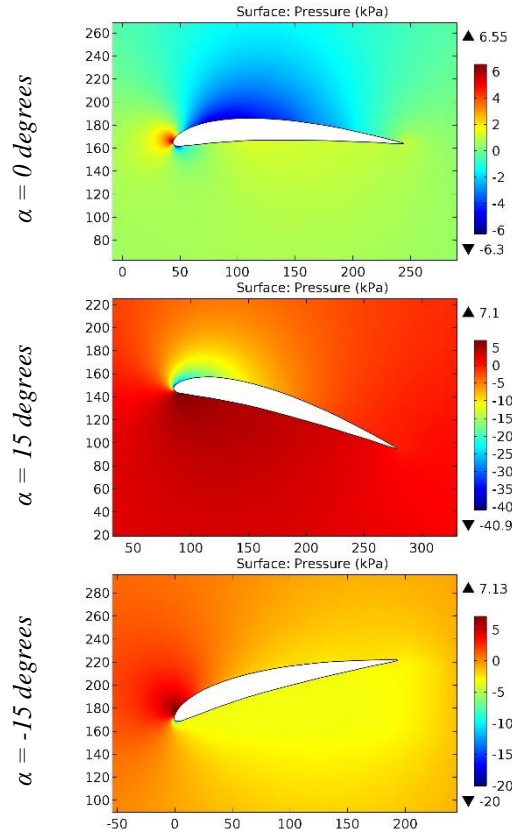


Figure 138. The pressure contours on the surfaces of the MVA-301 airfoil.

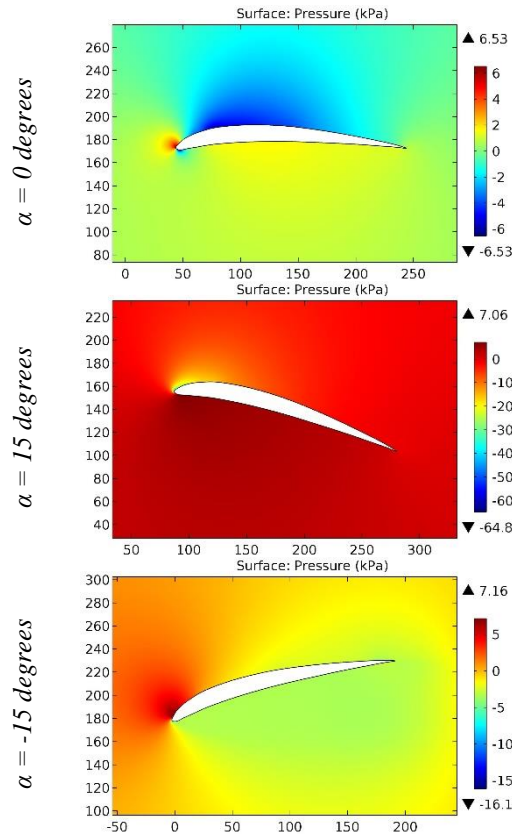


Figure 139. The pressure contours on the surfaces of the MVA30175 airfoil.

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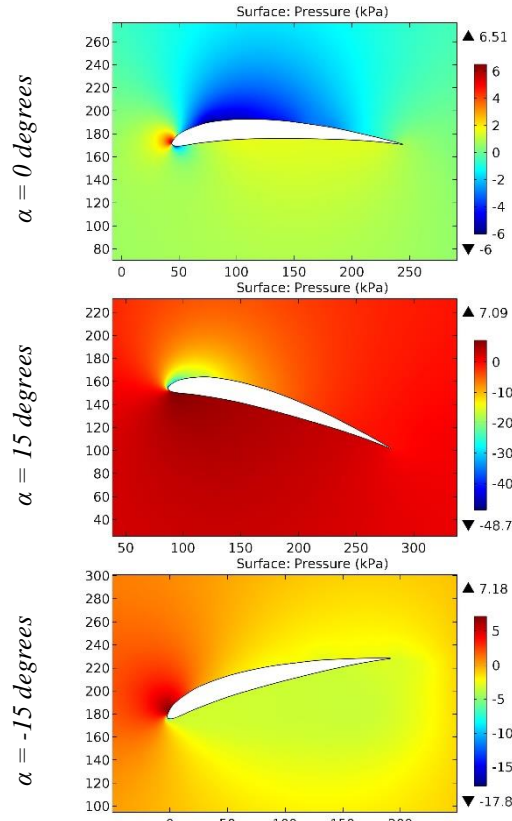


Figure 140. The pressure contours on the surfaces of the MVA-301M airfoil.

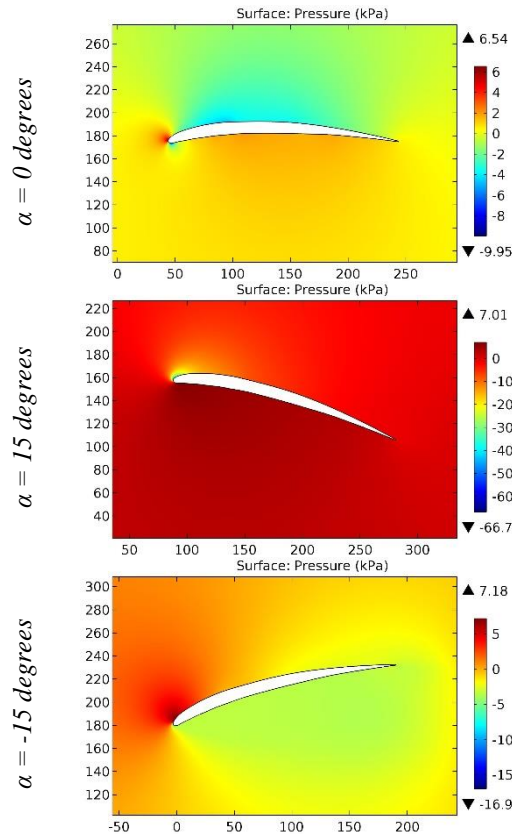


Figure 141. The pressure contours on the surfaces of the MVA-342 airfoil.

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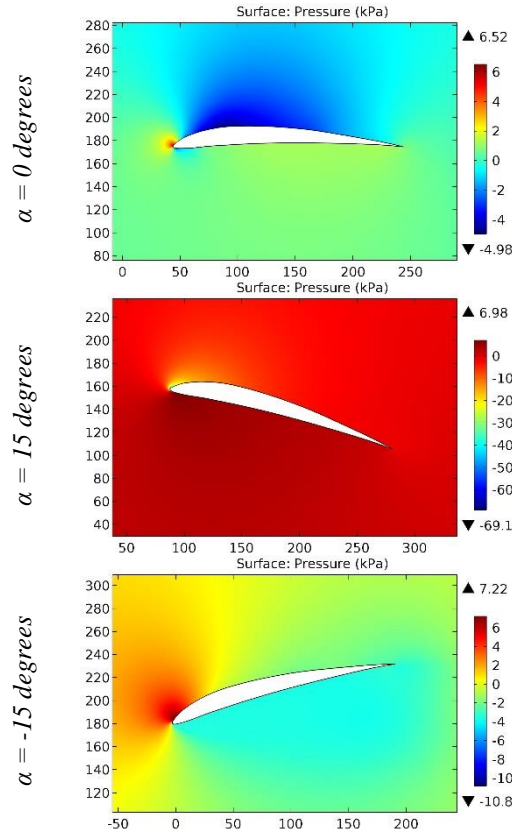


Figure 142. The pressure contours on the surfaces of the MVA-439 airfoil.

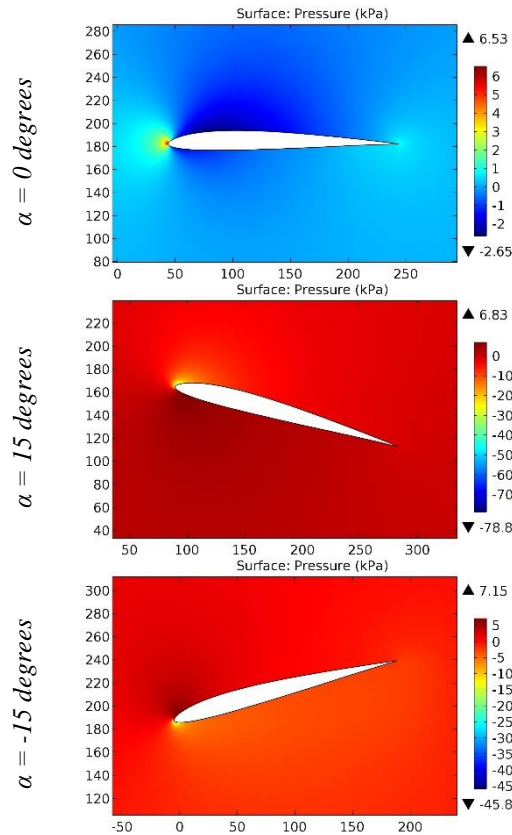


Figure 143. The pressure contours on the surfaces of the mve8.516 airfoil.

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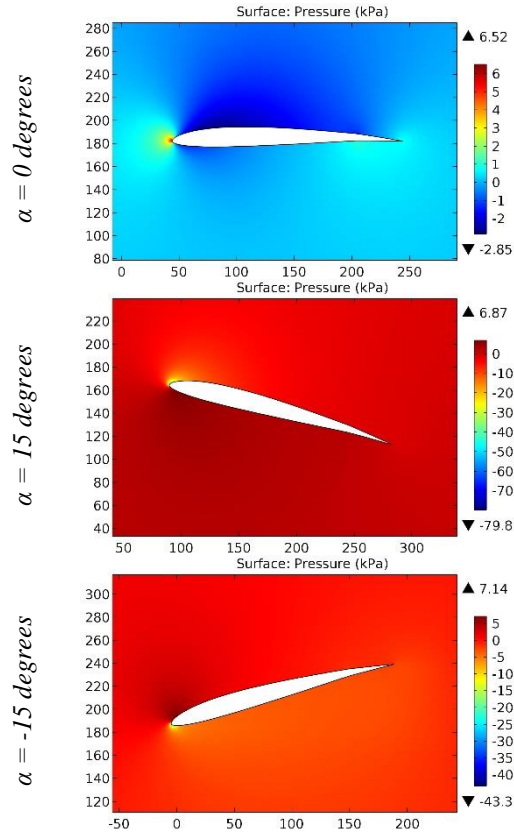


Figure 144. The pressure contours on the surfaces of the mve8516 f 3 airfoil.

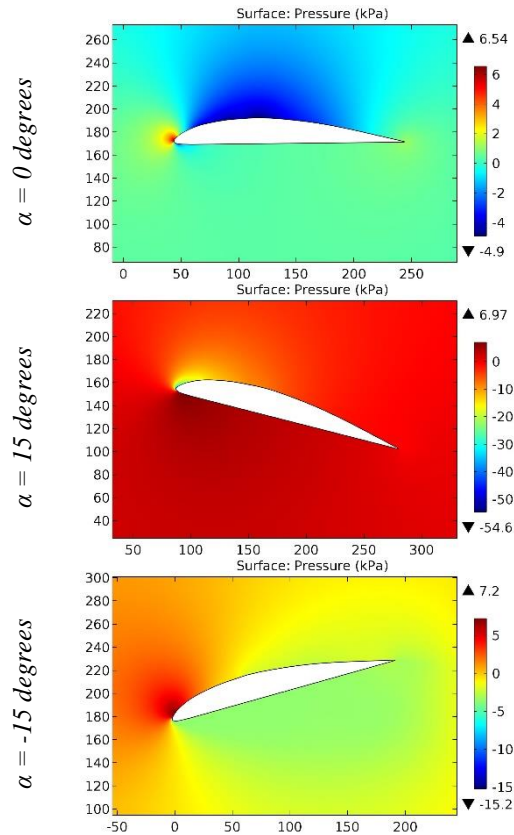


Figure 145. The pressure contours on the surfaces of the MZ 5411 airfoil.

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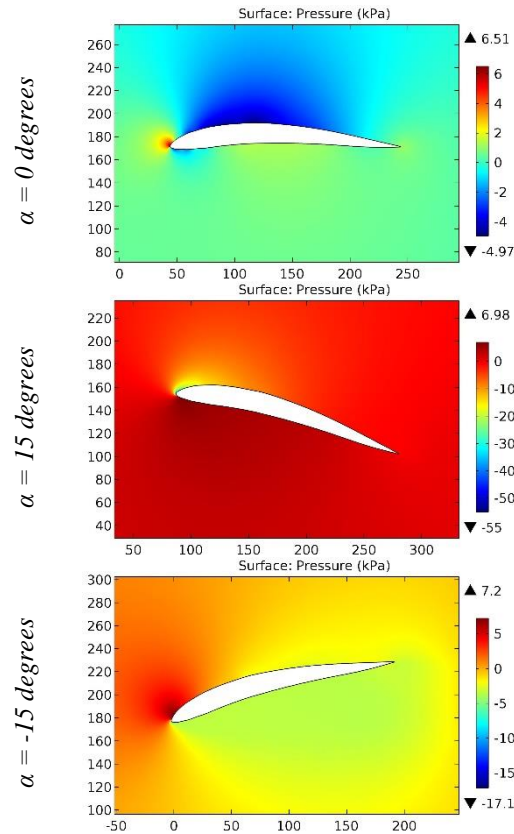


Figure 146. The pressure contours on the surfaces of the MZ 6409 airfoil.

Conclusion

Computer simulation makes it possible to determine the aerodynamic characteristics of the airplane wings under normal weather conditions. The presented calculated pressure contours, conjugated with the surfaces of the airfoils, create a complete picture of the influence of the geometry of the airfoil on the lift and drag value. Thus, the results of the calculation are relevant for choosing the advantageous

configuration of the airfoil of the airplane wing under certain flight conditions, for example, the development of the maximum speed of horizontal flight. For all the considered airfoils, the greatest value of positive pressure occurs during the airplane descent, and the greatest value of negative pressure occurs both during the airplane climb and during the airplane descent.

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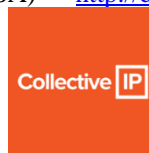
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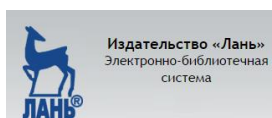
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