

Impact Factor:	ISRA (India)	= 6.317	SIS (USA)	= 0.912	ICV (Poland)	= 6.630
	ISI (Dubai, UAE)	= 1.582	ПИИИ (Russia)	= 0.191	PIF (India)	= 1.940
	GIF (Australia)	= 0.564	ESJI (KZ)	= 8.100	IBI (India)	= 4.260
	JIF	= 1.500	SJIF (Morocco)	= 7.184	OAJI (USA)	= 0.350

SOI: [1.1/TAS](https://s-o-i.org/1.1/TAS) DOI: [10.15863/TAS](https://dx.doi.org/10.15863/TAS)

International Scientific Journal
Theoretical & Applied Science

p-ISSN: 2308-4944 (print) e-ISSN: 2409-0085 (online)

Year: 2025 Issue: 02 Volume: 142

Published: 27.02.2025 <http://T-Science.org>

Issue

Article



Mukhiddin Khudjaev
Tashkent State Transport University
Professor, Tashkent, Uzbekistan
mukhiddinkhudjaev@gmail.com

Gulomjon Pirnazarov
Tashkent State Transport University
Head of department, Tashkent, Uzbekistan

Shexroz Ibrohimov
Tashkent State Transport University
Assistant, Tashkent, Uzbekistan

Javokhirbek Temirov
Tashkent State Transport University
Assistant, Tashkent, Uzbekistan

Sarvarbek Ma'murjonov
Tashkent State Transport University
Assistant, Tashkent, Uzbekistan

GENERALIZED FORMULAS FOR FRICTION FORCE AND CONSTRAINT REACTION FORCE OF A HORIZONTAL AXISYMMETRIC WEDGE

Abstract: The article studies the static state of an axisymmetric wedge. The static problem is solved using classical mechanics methods. The constraints are replaced by reaction forces. The equations of the wedge equilibrium state are derived. Generalized formulas for the friction force and the constraint reaction force of the wedge are obtained. A comparative analysis of the calculations is conducted.

Key words: wedge, friction force, constraint reaction forces, equilibrium equation.

Language: English

Citation: Khudjaev, M., Pirnazarov, G., Ibrohimov, Sh., Temirov, J., & Ma'murjonov, S. (2025). Generalized formulas for friction force and constraint reaction force of a horizontal axisymmetric wedge. *ISJ Theoretical & Applied Science*, 02 (142), 103-106.

Soi: <https://s-o-i.org/1.1/TAS-02-142-18> **Doi:**  <https://dx.doi.org/10.15863/TAS.2025.02.142.18>

Scopus ASCC: 2200.

Introduction

Wedge-shaped working bodies are used in many industries. Determining the unknown friction forces and constraint reaction forces of the wedge is a relevant problem.

A generalized model of a wedge-shaped spring-friction set of a freight car bogie was developed in [1]. Critically discussing the lack of classical mechanics methods in numerous publications, the equation of

equilibrium of friction wedges was derived according to the principle of release from restraints and an analytical expression of the reaction of a friction wedge was obtained [2]. A mathematical model of a wedge clutch was developed considering sliding friction [3].

A theory of a dihedral wedge widely used in agricultural research was created in [4]. Calculations were conducted based on this theory and the results

Impact Factor:

ISRA (India) = 6.317
ISI (Dubai, UAE) = 1.582
GIF (Australia) = 0.564
JIF = 1.500

SIS (USA) = 0.912
ПИИИ (Russia) = 0.191
ESJI (KZ) = 8.100
SJIF (Morocco) = 7.184

ICV (Poland) = 6.630
PIF (India) = 1.940
IBI (India) = 4.260
OAJI (USA) = 0.350

obtained were compared, certifying the reliability of the formulas derived by this theory [5].

In this article, generalized formulas for the friction force and the restraint reaction force of an axisymmetric wedge are obtained.

Material

Consider the statics of penetration of a horizontal axisymmetric wedge into a homogeneous medium under constant force $\bar{P}$. We determine the friction

and reaction forces of the wedge using methods of theoretical mechanics [6, 7].

On the wedge surfaces in contact with the medium, friction forces $\bar{F}_{1fr}$ and $\bar{F}_{2fr}$, directed along the working planes of the wedge, are formed. The reaction forces of the medium $\bar{N}_1$ and $\bar{N}_2$ are directed perpendicular to these planes (Fig. 1).

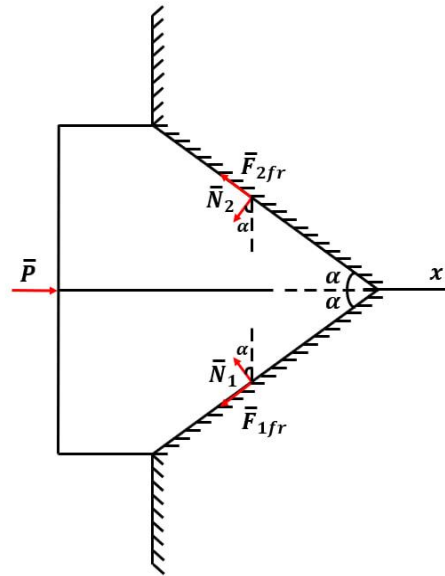


Fig. 1. Wedge shape and forces applied to it

Let us derive an equilibrium equation for the wedge, equating to zero the sum of all projections of the forces applied to the wedge on the x -axis:

$$P - N_1 \sin \alpha - F_{1fr} \cos \alpha - N_2 \sin \alpha - F_{2fr} \cos \alpha = 0. \quad (1)$$

From (1), with equalities $N_1 = N_2 = N$, $F_{1fr} = F_{2fr} = F_{fr}$ for an axisymmetric wedge and considering the Coulomb formula $F_{fr} = fN$ [6], we obtain $fP = 2F_{fr}(\sin \alpha - 2f \cos \alpha)$.

From here, we determine the friction force and, with $F_{fr} = fN$, the constraint reaction force of the wedge:

$$F_{fr} = \frac{fP}{2(\sin \alpha + f \cos \alpha)}, \quad (2)$$

$$N = \frac{P}{2(\sin \alpha + f \cos \alpha)}. \quad (3)$$

Here, f - is the friction coefficient.

Thus, expressions for the friction force and the restraint reaction force of the horizontal axisymmetric wedge are obtained. Using these formulas, we can determine the values of the friction and reaction forces at an arbitrary angle of inclination.

Results.

Using the solutions obtained, calculations were conducted for values $f = 0,2$ (coefficient of friction between steel and crushed stone) and $f = 0,4$ (coefficient of friction between steel and soil) for different values of applied force $\bar{P}$.

Figure 2 shows the results of calculating the constraint reaction force depending on the angle of inclination of the wedge at an applied force $P = 100$ N. The graphs in Fig. 2a were plotted for $f = 0,2$;

Impact Factor:

ISRA (India) = 6.317
ISI (Dubai, UAE) = 1.582
GIF (Australia) = 0.564
JIF = 1.500

SIS (USA) = 0.912
ПИИИ (Russia) = 0.191
ESJI (KZ) = 8.100
SJIF (Morocco) = 7.184

ICV (Poland) = 6.630
PIF (India) = 1.940
IBI (India) = 4.260
OAJI (USA) = 0.350

and the graphs in Fig. 2b correspond to $f = 0,4$. The graph with a solid line was obtained for the value of the reaction force by formula $N = P / \sin \alpha$ [6, 7, 8, 9] and from a wedge inclination angle of $\alpha = 10^\circ$, its

value tends to infinity. Another line was obtained by the formula derived by the authors of this article (3), according to which the reaction force has a numerical value at any value of the angle. A two times increase in the friction coefficient led to an increase in the value of the reaction force in the corresponding ratio.

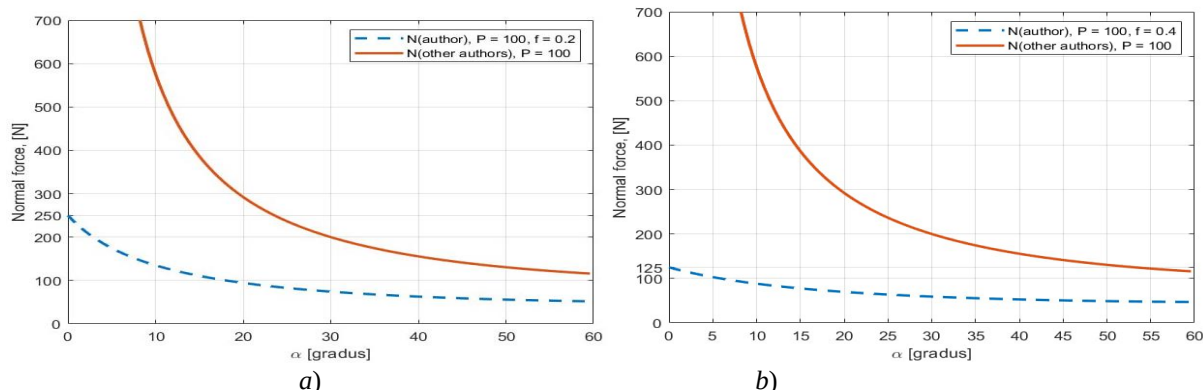


Fig. 2. Change in the reaction force depending on the angle of inclination of the wedge.

Figure 3 shows the results of friction force calculations for the value of the friction coefficient $f = 0,2$ for $P = 200$ N (a) and for $f = 0,2$; $P = 100$ N (b). The solid line is obtained by formula

$F_{fr} = Pf / \sin \alpha$ [6, 7, 8, 9] and it is clear that for $\alpha = 0$, the value of the friction force tends to infinity. The other line is obtained by formula (2) and here the friction force has a specific numerical value.

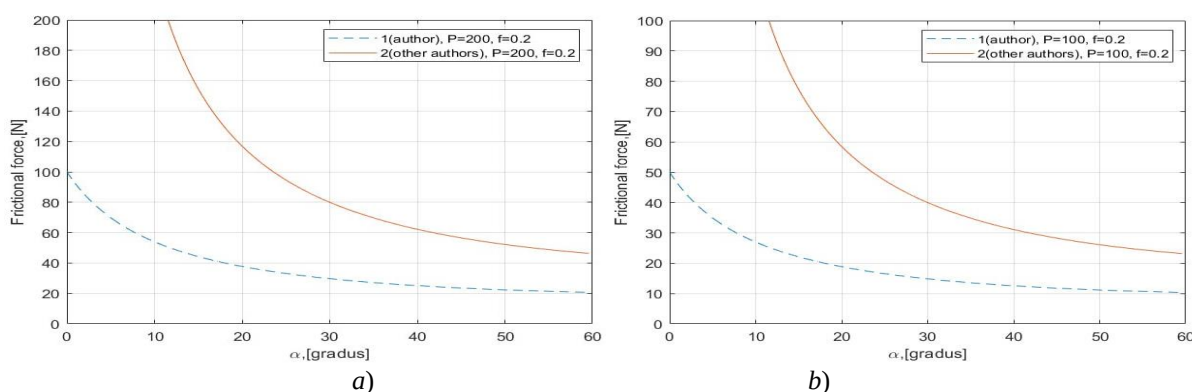


Fig. 3. Change in the friction force depending on the angle of inclination of the wedge.

Conclusion.

Analytical expressions for the friction and reaction forces of an axisymmetric wedge are obtained. These forces have specific numerical values

for all values of the angle of inclination of the wedge. Solutions obtained present generalized expressions of the friction force and the constraint reaction force of an axisymmetric wedge.

References:

1. Turanov, Kh.T. (2009). Generalized model of a spring-friction set of a freight car bogie. *Transport: Science, technology and management*. 2009. №12. pp. 32-36.
2. Turanov, Kh.T. (2013). *My scientific laboratory in mechanics*. (p.240). Yekaterinburg.
3. JianYao, Li Chen, & Chengliang Yin. (2014). Modeling and Stability Analysis of Wedge Clutch System. *Mathematical Problems in Engineering*. Volume 2014. Article ID 712472, <https://doi.org/10.1155/2014/712472>

Impact Factor:	ISRA (India)	= 6.317	SIS (USA)	= 0.912	ICV (Poland)	= 6.630
	ISI (Dubai, UAE)	= 1.582	ПИИИ (Russia)	= 0.191	PIF (India)	= 1.940
	GIF (Australia)	= 0.564	ESJI (KZ)	= 8.100	IBI (India)	= 4.260
	JIF	= 1.500	SJIF (Morocco)	= 7.184	OAJI (USA)	= 0.350

4. Goryachkin, V.P. (1968). *Collected works*. Volume 2, (p.455). Moscow: Kolos.
5. Gureev, I.I. (2019). Using a wedge for soil cultivation in adaptive agricultural technologies. *Journal "Bulletin of the Kursk State Agricultural Academy"*. 2019. pp. 34-38.
6. Yablonsky, A.A., & Nikiforova, V.M. (2002). *Course of theoretical mechanics*. (p.764). SPb.: Lan.
7. Szolga, V.I. (2013). «Theoretical mechanics», Berlin, part-1, 2013, 204 p.
8. Artobolevsky, I.I. (1988). *Theory of mechanisms and machines*. (p.640). Moscow: Nauka.
9. Frolov, K.V., & Popov, S.A. (2005). *Theory of mechanisms and machines*. (p.496). Moscow: Higher school.